

BRINE DISPOSAL WELL PERMIT APPLICATION BITTINGER #3

Bear Lake Properties, LLC

March 2015

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CLEAR SOLUTIONS"



March 24, 2015

S. Stephen Platt U.S. EPA Region III Ground Water & Enforcement Branch (3WP22) 1650 Arch Street Philadelphia, PA 19103

Subject: Application For Underground Injection Control Class II-D Brine Disposal Well Bear Lake Properties Bittinger #3 Well, Warren County, Pennsylvania

Dear Mr. Platt:

Enclosed please find two (2) copies of the Underground Injection Control Class II-D Brine Disposal Well permit application for the Bear Lake Properties, LLC (Bear Lake Properties) Bittinger #3 well located in Columbus Township, Warren County, Pennsylvania. As indicated in Section 10 "Necessary Resources", Bear Lake Properties will provide under separate cover the Certificate of Deposit to verify they have the necessary resources to properly plug and abandon the well.

Your prompt review of the application would be greatly appreciated. Please feel free to contact Karl Kimmich of Bear Lake Properties at (724) 444-7501 or me at (412) 921-4006 if you have questions or comments.

Sincerely, Tetra Tech, Inc.

Dale E. Skoff, P.G. Sr. Project Manager

cc: Dave Rectenwald – EPA

Karl Kimmich – Bear Lake Properties

John Holko – Bear Lake Properties

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EPA Form 7520-6 Rev. 12-08)

Well Class and Type Codes

Class I Wells used to inject waste below the deepest underground source of drinking

water.

Type "I" Nonhazardous industrial disposal well

"M" Nonhazardous municipal disposal well

"W" Hazardous waste disposal well injecting below USDWs

"X" Other Class I wells (not included in Type "I," "M," or "W")

Class II Oil and gas production and storage related injection wells.

Type "D" Produced fluid disposal well

"R" Enhanced recovery well

"H" Hydrocarbon storage well (excluding natural gas)

"X" Other Class II wells (not included in Type "D," "R," or "H")

Class III Special process injection wells.

Type "G" Solution mining well

"S" Sulfur mining well by Frasch process

"U" Uranium mining well (excluding solution mining of conventional mines)

"X" Other Class III wells (not included in Type "G," "S," or "U")

Other Classes Wells not included in classes above.

Class V wells which may be permitted under §144.12. Wells not currently classified as Class I, II, III, or V.

Attachments to Permit Application

Class Attachments I new well A, B, C, D, F, H – S, U existing A, B, C, D, F, H – U II new well A, B, C, E, G, H, M, Q, R; optional – I, J, K, O, P, U existing A, E, G, H, M, Q, R, – U; optional – J, K, O, P, Q III new well A, B, C, D, F, H, I, J, K, M – S, U existing A, B, C, D, F, H, J, K, M – U

Other Classes

To be specified by the permitting authority

INSTRUCTIONS - Underground Injection Control (UIC) Permit Application

Paperwork Reduction Act: The public reporting and record keeping burden for this collection of information is estimated to average 224 hours for a Class I hazardous well application, 110 hours for a Class I non-hazardous well application, 67 hours for a Class II well application, and 132 hours for a Class III well application. Burden means the total time, effort, or financial resource expended by ersons to generate, maintain, retain, or disclose or provide information to or for a Federal Agency. This includes the time needed to review instructions; develop, acquire, install, and utilize technology and systems for the purposes of collecting, validating, and verifying information, processing and maintaining information, and disclosing and providing information; adjust the existing ways to comply with any previously applicable instructions and requirements; train personnel to be able to respond to the collection of information; search data sources; complete and review the collection of information; and, transmit or otherwise disclose the information. An agency may not conduct or sponsor, and a person is not required to respond to, a collection of information unless it displays a currently valid OMB control number. Send comments on the Agency's need for this information, the accuracy of the provided burden estimates, and any suggested methods for minimizing respondent burden, including the use of automated collection techniques to Director, Collection Strategies Division, U.S. Environmental Protection Agency (2822), 1200 Pennsylvania Ave., NW, Washington, DC 20460. Include the OMB control number in any correspondence. Do not send the completed forms to this address.

This form must be completed by all owners or operators of Class I, II, and III injection wells and others who may be directed to apply for permit by the Director.

- I. EPA I.D. NUMBER Fill in your EPA Identification Number. If you do not have a number, leave blank.
- II. OWNER NAME AND ADDRESS Name of well, well field or company and address.
- III. OPERATOR NAME AND ADDRESS Name and address of operator of well or well field.
- IV. COMMERCIAL FACILITY Mark the appropriate box to indicate the type of facility.
- V. OWNERSHIP Mark the appropriate box to indicate the type of ownership.
- VI. LEGAL CONTACT Mark the appropriate box.
- VII. SIC CODES List at least one and no more than four Standard Industrial Classification (SIC) Codes that best describe the nature of the business in order of priority.
- VIII. WELL STATUS Mark Box A if the well(s) were operating as injection wells on the effective date of the UIC Program for the State. Mark Box B if wells(s) existed on the effective date of the UIC Program for the State but were not utilized for injection. Box C should be marked if the application is for an underground injection project not constructed or not completed by the effective date of the UIC Program for the State.
- IX. TYPE OF PERMIT Mark "Individual" or "Area" to indicate the type of permit desired. Note that area permits are at the discretion of the Director and that wells covered by an area permit must be at one site, under the control of one person and do not inject hazardous waste. If an area permit is requested the number of wells to be included in the permit must be specified and the wells described and identified by location. If the area has a commonly used name, such as the "Jay Field," submit the name in the space provided. In the case of a project or field which crosses State lines, it may be possible to consider an area permit if EPA has jurisdiction in both States. Each such case will be considered individually, if the owner/operator elects to seek an area permit.
- X. CLASS AND TYPE OF WELL Enter in these two positions the Class and type of injection well for which a permit is requested. Use the most pertinent code selected from the list on the reverse side of the application. When selecting type X please explain in the space provided.
- XI. LOCATION OF WELL Enter the latitude and longitude of the existing or proposed well expressed in degrees, minutes, and seconds or the location by township, and range, and section, as required by 40 CFR Part 146. If an area permit is being requested, give the latitude and longitude of the approximate center of the area.
- XII. INDIAN LANDS Place an "X" in the box if any part of the facility is located on Indian lands.
- **ATTACHMENTS** Note that information requirements vary depending on the injection well class and status. Attachments for Class I, II, III are described on pages 4 and 5 of this document and listed by Class on page 2. Place EPA ID number in the upper right hand corner of each page of the Attachments.
- XIV. CERTIFICATION All permit applications (except Class II) must be signed by a responsible corporate officer for a corporation, by a general partner for a partnership, by the proprietor of a sole proprietorship, and by a principal executive or ranking elected official for a public agency. For Class II, the person described above should sign, or a representative duly authorized in writing.

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INSTRUCTIONS - Attachments

Attachments to be submitted with permit application for Class I, II, III and other wells.

- A. AREA OF REVIEW METHODS Give the methods and, if appropriate, the calculations used to determine the size of the area of review (fixed radius or equation). The area of review shall be a fixed radius of 1/4 mile from the well bore unless the use of an equation is approved in advance by the Director.
- B. MAPS OF WELL/AREA AND AREA OF REVIEW Submit a topographic map, extending one mile beyond the property boundaries, showing the injection well(s) or project area for which a permit is sought and the applicable area of review. The map must show all intake and discharge structures and all hazardous waste treatment, storage, or disposal facilities. If the application is for an area permit, the map should show the distribution manifold (ifapplicable) applying injection fluid to all wells in the area, including all system monitoring points. Within the area of review, the map must show the following:

Class I

The number, or name, and location of all producing wells, injection wells, abandoned wells, dryholes, surface bodies of water, springs, mines (surface and subsurface), quarries, and other pertinent surface features, including residences and roads, and faults, if known or suspected. In addition, the map must identify those wells, springs, other surface water bodies, and drinking water wells located within one quarter mile of the facility property boundary. Only information of public record is required to be included in this map;

Class II

In addition to requirements for Class I, include pertinent information known to the applicant. This requirement does not apply to existing Class II wells;

Class III

In addition to requirements for Class I, include public water systems and pertinent information known to the applicant.

C. CORRECTIVE ACTION PLAN AND WELL DATA - Submit a tabulation of data reasonably available from public records or otherwise known to the applicant on all wells within the area of review, including those on the map required in B, which penetrate the proposed injection zone. Such data shall include the following:

Class I

Adescription of each well's types, construction, date drilled, location, depth, record of plugging and/or completion, and any additional information the Director may require. In the case of new injection wells, include the corrective action proposed to be taken by the applicant under 40 CFR 144.55.

Class II

In addition to requirement for Class I, in the case of Class II wells operating over the fracture pressure of the injection formation, all known wells within the area of review which penetrate formations affected by the increase in pressure. This requirement does not apply to existing Class II wells.

Class III

In addition to requirements for Class I, the corrective action proposed under 40 CFR 144.55 for all Class III wells.

D. MAPS AND CROSS SECTION OF USDWs - Submit maps and cross sections indicating the vertical limits of all underground sources of drinking water within the area of review (both vertical and lateral limits for Class I), their position relative to the injection formation and the direction of water movement, where known, in every underground source of drinking water which may be affected by the proposed injection. (Does not apply to Class II wells.)

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- E NAME AND DEPTH OF USDWs (CLASS II) For Class II wells, submit geologic name, and depth to bottom of all underground sources of drinking water which may be affected by the injection.
- F. MAPS AND CROSS SECTIONS OF GEOLOGIC STRUCTURE OF AREA Submit maps and cross sections detailing the geologic structure of the local area (including the lithology of injection and confining intervals) and generalized maps and cross sections illustrating the regional geologic setting. (Does not apply to Class II wells.)
- GEOLOGICAL DATA ON INJECTION AND CONFINING ZONES (Class II) For Class II wells, submit appropriate geological data on the injection zone and confining zones including lithologic description, geological name, thickness, depth and fracture pressure.
- H. OPERATING DATA Submit the following proposed operating data for each well (including all those to be covered by area permits): (1) average and maximum dailyrate and volume of the fluids to be injected; (2) average and maximum injection pressure; (3) nature of annulus fluid; (4) for Class I wells, source and analysis of the chemical, physical, radiological and biological characteristics, including density and corrosiveness, of injection fluids; (5) for Class II wells, source and analysis of the physical and chemical characteristics of the injection fluid; (6) for Class III wells, a qualitative analysis and ranges in concentrations of all constituents of injected fluids. If the information is proprietary, maximum concentrations only may be submitted, but all records must be retained.
- FORMATION TESTING PROGRAM Describe the proposed formation testing program. For Class I wells the program must be designed to obtain data on fluid pressure, temperature, fracture pressure, other physical, chemical, and radiological characteristics of the injection matrix and physical and chemical characteristics of the formation fluids.

For Class II wells the testing program must be designed to obtain data on fluid pressure, estimated fracture pressure, physical and chemical characteristics of the injection zone. (Does not apply to existing Class II wells or projects.)

For Class III wells the testing must be designed to obtain data on fluid pressure, fracture pressure, and physical and chemical characteristics of the formation fluids if the formation is naturally water bearing. Only fracture pressure is required if the program formation is not water bearing. (Does not apply to existing Class III wells or projects.)

- J. STIMULATION PROGRAM Outline any proposed stimulation program.
- K. INJECTION PROCEDURES Describe the proposed injection procedures including pump, surge, tank, etc.
- L. CONSTRUCTION PROCEDURES Discuss the construction procedures (according to §146.12 for Class I, §146.22 for Class II, and §146.32 for Class III) to be utilized. This should include details of the casing and cementing program, logging procedures, deviation checks, and the drilling, testing and coring program, and proposed annulus fluid. (Request and submission of justifying data must be made to use an alternative to packer for Class I.)
- M. CONSTRUCTION DETAILS Submit schematic or other appropriate drawings of the surface and subsurface construction details of the well.
- N. CHANGES IN INJECTED FLUID Discuss expected changes in pressure, native fluid displacement, and direction of movement of injection fluid. (Class III wells only.)
- O. PLANS FOR WELL FAILURES Outline contingency plans (proposed plans, if any, for Class II) to cope with all shut-ins or wells failures, so as to prevent migration of fluids into any USDW.
- P. MONITORING PROGRAM Discuss the planned monitoring program. This should be thorough, including maps showing the number and location of monitoring wells as appropriate and discussion of monitoring devices, sampling frequency, and parameters measured. If a manifold monitoring program is utilized, pursuant to §146.23(b)(5), describe the program and compare it to individual well monitoring.
- Q. PLUGGING AND ABANDONMENT PLAN Submit a plan for plugging and abandonment of the well including: (1) describe the type, number, and placement (including the elevation of the top and bottom) of plugs to be used; (2) describe the type, grade, and quantity of cement to be used; and (3) describe the method to be used to place plugs, including the method used to place the well in a state of static equilibrium prior to placement of the plugs. Also for a Class III well that underlies or is in an exempted aquifer, demonstrate adequate protection of USDWs. Submit this information on EPA Form 7520-14, Plugging and Abandonment Plan.

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- **R. NECESSARY RESOURCES** Submit evidence such as a surety bond or financial statement to verify that the resources necessary to close, plug or abandon the well are available.
- S. AQUIFER EXEMPTIONS If an aquifer exemption is requested, submit data necessary to demonstrate that the aquifer meets the following criteria: (1) does not serve as a source of drinking water; (2) cannot now and will not in the future serve as a source of drinking water; and (3) the TDS content of the ground water is more than 3,000 and less than 10,000 mg/l and is not reasonably expected to supply a public water system. Data to demonstrate that the aquifer is expected to be mineral or hydrocarbon production, such as general description of the mining zone, analysis of the amenability of the mining zone to the proposed method, and time table for proposed development must also be included. For additional information on aquifer exemptions, see 40 CFR Sections 144.7 and 146.04.
- T. **EXISTING EPA PERMITS** List program and permit number of any existing EPA permits, for example, NPDES, PSD, RCRA, etc.
- U. DESCRIPTION OF BUSINESS Give a brief description of the nature of the business.

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Section 1 – Area of Review Methods/Calculations



45610 Woodland Road, Suite 400, Sterling, VA 20166 703-444-7000 703-444-1685 (FAX)

TECHNICAL MEMORANDUM

TO: Dale Skoff, Tetra Tech OGA

FROM: Jeffrey Benegar

DATE: February 4, 2015

RE: Area of Review/Zone of Endangerment Analysis for Bittinger #3 and Smith-Ras #1

Wells – Bear Lake Properties

EXECUTIVE SUMMARY

This technical memorandum (TM) summarizes the analytical modeling we have performed for the area of review/zone of endangerment analysis for the Bittinger #3 and Smith-Ras #1 wells. The scenarios involved injecting simultaneously at existing Bear Lake Properties UIC Class IID brine disposal wells Bittinger #1, #4, and #2, all of which are located in Columbus Township, Warren County, Pennsylvania (the Bittinger #1 and Bittinger #4 wells received their final UIC Class IID (Commercial) well permits in November 2012 and Bittinger #2 in late 2014). The relevant parameters for our analysis were obtained from Bear Lake Properties, LLC or estimated in the absence of any information. Our analysis is described in more detail below.

OVERVIEW AND METHODOLOGY

There are several methods proposed for calculating the zone of endangerment of an injection well. The most simplistic method is the use of a fixed radius, based on the type of injection well being permitted. Other methods involve calculation of the radius based on well and formation properties. Most regulatory agencies require the use of calculations to determine the zone of endangerment. The method used here is the graphical method first used by US EPA Region 6. It involves the calculation of the increase of pressure in the formation due to injection, then converting that pressure into equivalent feet of head. The increase in head in the formation due to injection is then compared to the equivalent head of the lowest most underground source of drinking water (USDW). When plotted graphically, the intersection of those two curves at some distance, r, determines the radius of the zone of endangerment.

The increase in pressure in the formation due to injection depends on the properties of the injection fluid and the formation, the rate of fluid injection, and the length of time of injection. The most common mathematical expression to describe this increase in pressure was developed

by Matthews and Russell (1967). Matthews and Russell assume that, for a single well injecting into an infinite, homogeneous and isotropic, non-leaking formation, the increase in pressure (delta p) can be described as:

delta p = $162.6 \text{ Q}\mu / \text{kh} * [(\log(\text{kt} / \Phi \mu \text{Cr}^2) - 3.23] \text{ where:}$

delta p = pressure change (psi) at radius, r and time, t

Q = injection rate (barrels/day)

 μ = injectate viscosity (centipoise)

k = formation permeability (millidarcies)

h = formation thickness (feet)

t = time since injection began (hours)

C = compressibility (total, sum of water and rock compressibility) (psi⁻¹)

r = radial distance from wellbore to point of investigation (feet)

 Φ = average formation porosity (decimal)

PARAMETERS USED IN THE ANALYSIS

The following parameters were used in the zone of endangerment analysis. For injection rate, we used the average daily rate based on the permitted monthly rate for the three existing permitted Bear Lake Properties UIC Class IID wells, which is 30,000 bbls/month for each well, which averages approximately 1,000 bbls/day per well. For permeability, we used a value of 50 md, which we feel is conservative based on the injection rate sustainable for existing disposal wells at the site and the substantial volume of natural gas produced from the reservoir, both of which indicate significant permeability. The initial pressure at the top of the injection formation was based upon measurements taken prior to injection at the Bittinger #4 well.

Bittinger #3 Medina Group Well

Q = 1000 barrels/day

t = 10 years = 87,600 hours

 $\mu = 1$ centipoise

k = 50 md

h = 61 feet

 $C = 3.0e-06 \text{ psi}^{-1}$

 $\Phi = 0.08$

Specific gravity of injectate = 1.218

Surface elevation = 1638 feet

Depth to injection formation = 4260 feet

Base of lowest most USDW (MSL) = 1338 feet

Initial pressure at top of injection formation = 128 psi

Smith-Ras #1 Medina Group Well

Q = 1000 barrels/day

t = 10 years = 87,600 hours

 $\mu = 1$ centipoise

k = 50 md

h = 61 feet

 $C = 3.0e-06 \text{ psi}^{-1}$

 $\Phi = 0.08$

Specific gravity of injectate = 1.218

Surface elevation = 1575 feet

Depth to injection formation = 4222 feet

Base of lowest most USDW (MSL) = 1275 feet

Initial pressure at top of injection formation = 128 psi

Bittinger #2 Medina Group Well

Q = 1000 barrels/day

t = 10 years = 87,600 hours

 $\mu = 1$ centipoise

k = 50 md

h = 61 feet

 $C = 3.0e-06 \text{ psi}^{-1}$

 $\Phi = 0.08$

Specific gravity of injectate = 1.218

Surface elevation = 1621 feet

Depth to injection formation = 4279 feet

Base of lowest most USDW (MSL) = 1321 feet

Initial pressure at top of injection formation = 128 psi

Bittinger #1 Medina Group Well

Q = 1000 barrels/day

t = 10 years = 87,600 hours

 $\mu = 1$ centipoise

k = 50 md

h = 61 feet

 $C = 3.0e-06 \text{ psi}^{-1}$

 $\Phi = 0.08$

Specific gravity of injectate = 1.218

Surface elevation = 1518 feet

Depth to injection formation = 4210 feet

Base of lowest most USDW (MSL) = 1218 feet

Initial pressure at top of injection formation = 128 psi

Bittinger #4 Medina Group Well

Q = 1000 barrels/day

t = 10 years = 87,600 hours

 $\mu = 1$ centipoise

k = 50 md

h = 61 feet

 $C = 3.0e-06 \text{ psi}^{-1}$

 $\Phi = 0.08$

Specific gravity of injectate = 1.218

Surface elevation = 1561 feet

Depth to injection formation = 4285 feet Base of lowest most USDW (MSL) = 1261 feet Initial pressure at top of injection formation = 128 psi

RESULTS

The Matthews and Russell equation was solved for various distances from the wellbore based on the parameters listed above. The distance between each of the wells is:

Wells	Distance (ft)
Bittinger #3 to Bittinger #2	2,052
Bittinger #3 to Bittinger #4	3,566
Bittinger #3 to Bittinger #1	3,779
Smith-Ras #1 to Bittinger #2	1,714
Smith-Ras #1 to Bittinger #4	2,584
Smith-Ras #1 to Bittinger #1	2,180
Smith-Ras #1 to Bittinger #3	1,980
Bittinger #1 to Bittinger #4	1,300
Bittinger #1 to Bittinger #2	2,000
Bittinger #2 to Bittinger #4	1,600

The Matthews and Russell equation was used to calculate the increase in pressure in the formation with only one well injecting. This was done for all five wells. Then, the calculated pressures for each well were added together and this sum was added to the value of existing pressure in the injection formation to obtain the total pressure in the formation when all five wells are injecting.

These values were then converted to feet of head of formation brine. The values are plotted against distance from the wellbore and are shown in Figure 1 for the Bittinger #3 well and Figure 2 for the Smith-Ras #1 well. The plot shows the calculated pressure surface within the injection formation, measured as feet of head of formation brine above the top of the injection formation. Also shown is the head of the lowest most USDW. Where the two lines intersect, the radius of the zone of endangerment can be estimated. The results indicate that the increase in head in the formation due to injection will intersect the elevation of the lowestmost USDW at a distance of approximately 4 feet for the Bittinger #3 well and approximately 60 feet for the Smith-Ras #1 well. These distances are well within the ½ mile standard fixed radius for area of review/zone of endangerment.

CONCLUSIONS

Our analysis of the area of review/zone of endangerment for the Bittinger #3 and Smith-Ras #1 wells (injecting together with the Bittinger #2, #4, and #1 wells) is based on a methodology typically used by US EPA. Based on the results, we believe the Bittinger #3 and Smith-Ras #1 wells are excellent candidates for use as brine disposal wells. The increase in head in the formation due to injection intersects the elevation of the lowestmost USDW well within ½ mile

for each well. The standard fixed radius of ¼ mile can be used for the area of review/zone of endangerment for the Bittinger #3 and Smith-Ras #1 wells.

REFERENCES

Matthews, C.S., Russell, D.G., (1967) Pressure Buildup and Flow Tests in Wells, SPE Monograph Series, Volume 1, New York.

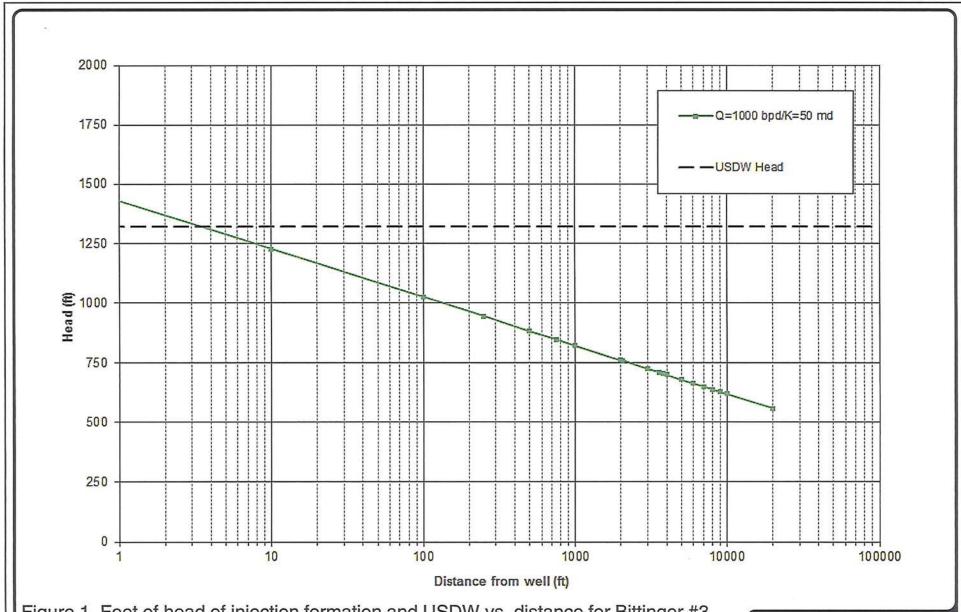


Figure 1. Feet of head of injection formation and USDW vs. distance for Bittinger #3 when all wells (Bittinger #2, #1, #4 and Smith-Ras #1) are injecting, K = 50 md



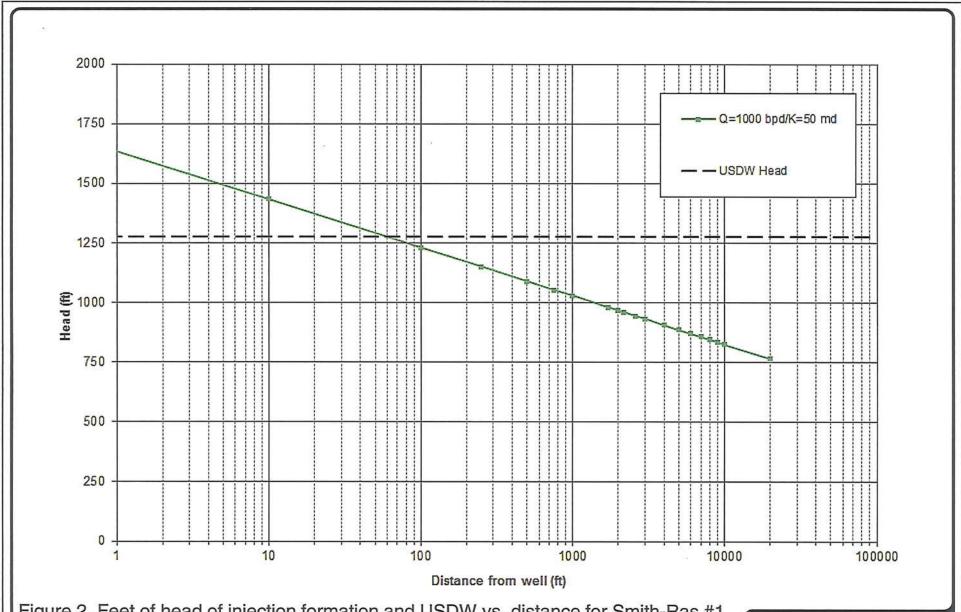


Figure 2. Feet of head of injection formation and USDW vs. distance for Smith-Ras #1 when all wells (Bittinger #2, #1, #4 and #3) are injecting, K = 50 md



Section 2 – Maps of Well Area and Area of Review

Section 2 – Maps of Well Area and Area of Review

According to publicly available records in the area, there are no intake or discharge structures, hazardous waste treatment, storage, or disposal facilities, mines, or quarries within one mile of the Bittinger #3 well. An intermittent unnamed tributary (UNT) to Tamarack Swamp is located approximately 1 mile southwest of the Bittinger #3 well. Tamarack Swamp is located approximately 1 mile southwest, Brokenstraw Creek is located approximately 1 mile northwest, and an UNT to Pine Valley Creek is located approximately 0.3 miles south of Bittinger #3.

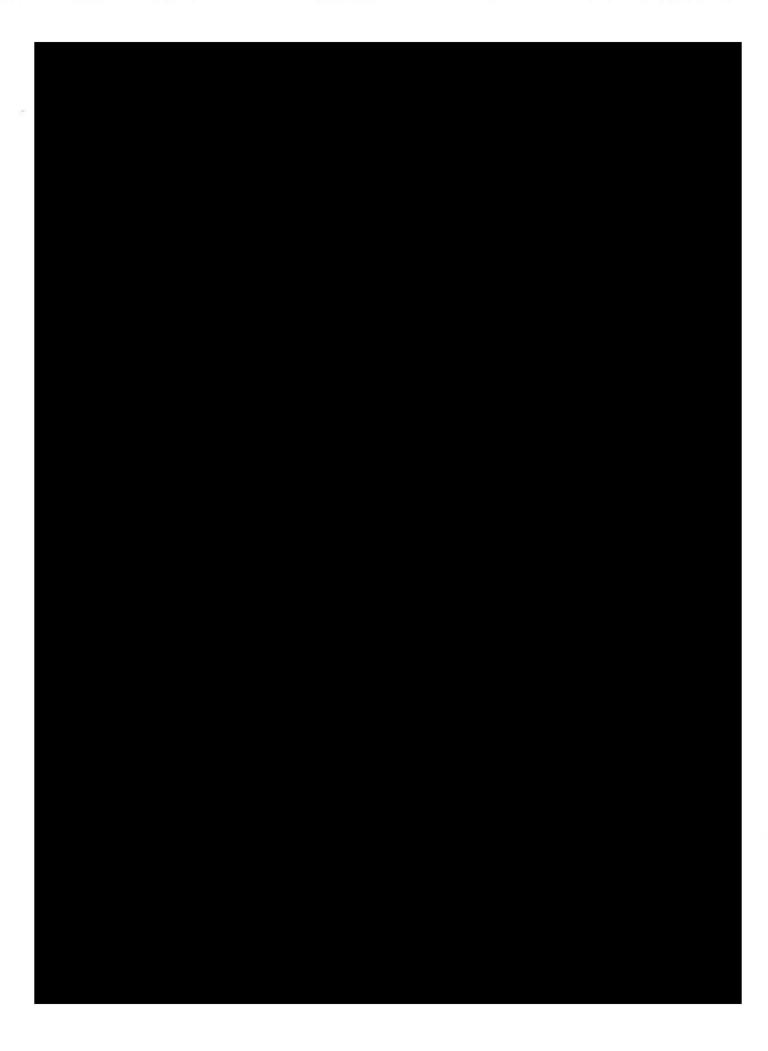
The Pennsylvania Geologic Survey "Ground Water Inventory System" (GWIS) database was accessed to determine the sources of groundwater sources in the site area. The database search identified one well within the quarter mile AOR. It is noted that the well reporting requirement was established in 1968 is not considered to be a complete record of water wells and other wells may be present. (Pennsylvania Topographic and Geologic Survey, September 15, 2010). In addition to the one well on the PA GWIS database, eight additional water wells were identified with the AOR based on public input and a foot survey by Bear Lake Properties staff. Attached are a map showing the location of the above-referenced wells and a table summarizing information on the wells.

The names and addresses of residents located within ¼ mile of the proposed injection well are provided in Appendix A.

Wells Located Within the 1/4 Mile Radius Area of Review (AOR) For The Bittinger #3 Well

Well Owner / Name API # Lat Long TD Completed Last Csg Csg depth Completion Oil and Gas and Proposed Injection Wells									
Bear Lake Properties Bittinger #3 (Proposed									
InjectionWell)	123-33945	41.996022	-79.528068	4566 ft	10/19/1984	4.5 in	4508 ft	Perf'd and frac'd	

AREA OF REVIEW MAPS
GROUNDWATER WELLS



Section 3 – Corrective Action Plan and Well Data

Section 3 - Corrective Action Plan and Well Data

According to publicly available records of oil and gas wells and a survey conducted by foot, there are no existing, or plugged and abandoned wells within the ¼ mile radius AOR for the Bittinger # 3 well. The R. Craker #1 and D. Wright #1 wells will be used as monitoring wells. If the fluid level in either monitoring well is observed to rise up to within 100 feet of the base of the USDW, disposal operations in the Bittinger #3 well will be stopped immediately, EPA will be notified, and operating conditions will be evaluated in order to control the fluid levels.

Existing Oil and Gas Wells within the Area of Review

Well completion records are required to be submitted for all wells located within the AOR in order to evaluate the need for corrective action specific to each well. As indicated above, there are no oil and gas wells located within the AOR.

Plugged and Abandoned Wells

No plugged and abandoned wells have been identified within the 1/4 mile AOR for the Bittinger #3 well.

Section 4 – Name and Depth of USDWs

Section 4 - Underground Sources of Drinking Water (USDW)

The site lies within the Glaciated Plateau section of the Appalachian Plateaus Physiographic province. Both unconsolidated glacial units and bedrock are used for potable water. The uppermost unit at the site is mapped as Wisconsin age glacial kame deposits. Kame deposits consist primarily of sand and gravel interbedded with minor amounts of silt and clay (Pennsylvania Topographic and Geologic Survey, 1959). The well log for Bittinger #3 indicates that unconsolidated gravel is present from the surface to a depth of 30 feet below ground surface.

The uppermost bedrock beneath the site is mapped as the Devonian age Venango formation. The Venango formation consists of interbedded pebble conglomerate, crossbedded sandstone, siltstone, and shale. This unit is up to 330 feet thick in Venango County; however, only a portion of the unit is present in the site area. This unit is used as an aquifer throughout Warren County. The well log for Bittinger #3 indicates that Devonian age shale is present from 30 ft to a depth of 2,816 ft below ground surface. This is believed to include the Venango Formation, the Chadokoin formation, and the underlying Bradford Group. Wells deeper than approximately 100 feet deep usually encounter salt water, which is supported by the generally shallow well depths in Columbus Township. (PADER, 1982, US Geologic Survey, 2007)

The Devonian age Chadakoin formation underlies Venango formation and consists of finegrained marine clastics (siltstone and shale) and includes a purplish pink sequence which is often used as a marker unit. This unit is up to 450 thick in Warren County.

The Pennsylvania Geologic Survey "Ground Water Inventory System" (GWIS) database was accessed to determine the sources of groundwater sources in the site area. The database search identified one well within the quarter mile AOR. It is noted that the well reporting requirement was established in 1968 is not considered to be a complete record of water wells and other wells may be present. (Pennsylvania Topographic and Geologic Survey, September 15, 2010). In addition to the one well on the PA GWIS database, eight additional water wells were identified within the AOR based on public input and a foot survey by Bear Lake Properties staff. Section 2 of this application includes a map showing the location of the above-referenced wells and a table summarizing information on the wells.

The New York Department of Environmental Conservation (DEC) "Water Well Program Information Search Wizard" website was utilized to determine if there were any water wells in New York State within the ¼ mile AOR of the Bittinger #3 well. No water wells were identified within the AOR of the Bittinger #3 well.

Based on the available information, the glacial units and the top 100 feet of bedrock is considered the underground sources of drinking water in the site area. The well logs indicate that the glacial material is approximately 30 feet thick beneath the site. Freshwater is expected to be encountered to a depth of approximately 100 feet with increasing salinity beyond that depth. The Bittinger #3 well has 8 5/8 inch surface casing cemented to a depth of 405 feet below ground surface, providing a buffer of approximately 300 feet beyond the base of the underground sources of drinking water based on the well data in Columbus Township (maximum well depth of 130 feet) and the references indicating brine being encountered at depths over 100 feet within the bedrock units. In addition, production casing extends several thousands of feet below the drinking water source and is cemented approximately 900 feet above the injection interval. (Injection well construction is described in detail in the "Well Construction" section.)

In calculating the depth to the base of the lowermost USDW, the depth of the deepest well in the area 130 feet (it is believed that the generally shallow well depth in the area was related to water quality issues based on the available literature) was doubled and rounded upward to the nearest 100 feet, providing a conservative maximum depth estimate of the underground source of drinking water of 300 feet.

References:

New York Department of Environmental Conservation website "DEC Water Well Program Information Search Wizard": http://www.dec.ny.gov/lands/33317.html

Pennsylvania Topographic and Geologic Survey, 1959. "Glacial Geology of Northwestern, PA." Bulletin G 32.

Pennsylvania Topographic and Geologic Survey, 1981. "Atlas of Preliminary Quadrangle Maps of Pennsylvania, PA." Map 61.

PADER, 1982. "Engineering Characteristics of the Rocks of Pennsylvania". Environmental Geology Report 1.

Pennsylvania Topographic and Geologic Survey, September 15/20, 2010. "Ground Water Inventory System". www.dcnr.state.pa.us/topogeo/groundwater/PAGWIS

US Geologic Survey, 2007. "Ground-Water Resources and the Hydrologic Effects of Petroleum Occurrence and Development, Warren County, Northwestern Pennsylvania." Scientific Investigations Report 2006-5263.

UNDERGROUND SOURCES OF DRINKING WATER BEDROCK MAP



BEDROCK MAP

JOSEPH BITTINGER 3 WELL

BEAR LAKE PROPERTIES, LLC

WARREN COUNTY, PENNSYLVANIA

DRAWN BY: S. PAXTON 01/28/15 CHECKED BY: D. SKOFF 03/23/15 APPROVED BY:

CONTRACT NUMBER: 212C-PB-00103

FIGURE NUMBER

REV

0

UNDERGROUND SOURCES OF DRINKING WATER GLACIAL MAP

Section 5 – Geologic Data on Injection and Confining Zones

Section 5 – Geologic Data on Injection and Confining Zones

The well is designed to inject into the Grimsby and Whirlpool sandstone units of the Medina Group which occurs at depths between 4,260 and 4,439 feet below grade in the Bittinger #3 well. The Medina is a depleted reservoir in this area.

As seen on the generalized stratigraphic column (attached), most of the geologic "groups" and "formations" overlying the Medina can be considered confining units totaling approximately 2,000 feet. Although many of these units are predominantly shale, they also contain reservoir rock and are shown with shading in confining unit column. Therefore, the Lockport and the Salina are seen as the most significant confining units and have a combined thickness of approximately 800 feet in the site area. As indicated, these units provide only a portion of the confining capacity and there are numerous other units that provide further protection.

The characteristics of the Medina Group formations including the Grimsby and Whirlpool are described in the attached report prepared by Billman Geologic Consultants entitled, "Geologic Review of the Bittinger Area, Planned SWD Site", dated August 2, 2010, and the cover letter dated April 5, 2014 discussing the Bittinger #2 well geologic characteristics. The subject report includes cross-sections in the vicinity of the Bittinger #3 well. As demonstrated by the cross-sections, the formation characteristics (lithology, thickness, porosity, etc.) of the Medina Group rocks in the Bittinger #3 well are very similar to those of the nearby wells including the three permitted brine disposal wells (Bittinger #1, #2 and #4 wells) operated by Bear Lake Properties.

Also attached are the following:

- Bittinger #3 completion record and geophysical log,
- Maximum Injection Pressure (MIP) calculations based on Instantaneous Shut-In Pressure (ISIP) data for the nearby Smith/Ras #1 well
- Smith/Ras #1 treatment reports.

Potential for Faults and Seismicity

As discussed in the attached Billman Geologic Consultants Report, geologic mapping performed at the Bear Lake Properties site as part of natural gas exploration and development in the Medina Group sandstone units has not identified evidence of significant faulting (e.g., duplicated intervals evident in log analysis, unusual thickening or thinning of intervals, etc.). Likewise the production of large volumes of natural gas from the Medina Group indicates the lack of significant faults which would allow for migration of the entrapped gas out of the Medina.

It is also noted that the Medina Group wells at the site are largely depleted resulting in lower than natural rock pressures. Production data for the Bittinger #3 are summarized on the attached table (referenced above) along with six other nearby wells. Cumulative gas production from the Bittinger #3 well is approximately 213 MMCF. Total production from all seven wells is over 1.75 BCF. The impact of removal of this large volume of gas is, as expected, a decrease in reservoir pressure. Injecting brine at or below the proposed maximum injection pressure would therefore not likely result in "overpressuring" faults (if any do exist in the area) and causing movement.

Finally, it is highly unlikely that injection at the site would engage any deep, Pre-Cambrian basement faults. According to the PA DCNR "Precambrian Basement Map of the Appalachian Basin and Piedmont Province in Pennsylvania" http://www.dcnr.state.pa.us/cs/groups/public/documents/document/dcnr 016250.pdf) the depth to

basement in the site vicinity is estimated at approximately 2,500 meters (or 8,200 feet) below sea level. The base of the Medina Group at the Bear Lake Properties site is approximately 2,800 ft. below sea level, or approximately a mile above Pre-Cambrian basement.

A review of the PA DCNR "Earthquake Epicenters in and Near Pennsylvania" (attached) indicates that there have been no recorded seismic events within 25 miles of the disposal project area since 1724, the start of the reporting period.

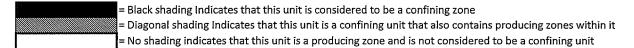
In summary, a detailed review of the zone of injection and data on geologic strata surrounding the zone of injection for the proposed brine disposal well, indicates the following supporting evidence that seismicity is highly unlikely: 1) The detailed geologic cross-sections (Appendix 2 of the Billman Geologic Consultants Report) and isopach and structural mapping completed by Billman Geologic Consultants show no evidence of faulting in the study area. 2) Historic production of over 1.75 billion cubic feet of gas among the Bittinger #1, #2, #3 and #4, Smith Ras #1 and Trisket #1 and #2 wells and unknown volumes of formation brine from the proposed zone of injection near the Bittinger #3 has depleted the zone of almost 90% of its original reservoir pressure. The disposal operations will re-fill this void space over the life of the project. 3) There have been no recorded seismic events within 25 miles of the disposal project area since 1724, the start of the reporting period referenced in the PA DCNR earthquake epicenters map.

GEOLOGIC DATA GENERALIZED STRATIGRAPHIC COLUMN

Generalized Stratigraphic Column Bittinger No 3 Warren County, PA

Age	Group	Formation	Predominant	Total Depth	Thickness	Confining
			Rock Type	to Base(Feet)	Feet	Zone
Glacial Units				30	30	
Upper Devonian	Venango		Shale/sandstone			
Upper Devonian		Chadakoin	Shale			
Upper Devonian	Bradford		Shale			
Upper Devonian	Elk		Shale	2816	2786	
Upper Devonian		Java	Shale	2010	2/00	
Upper Devonian		West Falls	Shale			
Upper Devonian		Sonyea	Shale			
Upper Devonian		Genesee	Shale			
Upper Devonian		Tully Limestone	Limestone	2926	110	
Upper Devonian	Hamilton	Mahantango	Shale, some sandstone	3097	171	
Upper Devonian	Hamilton	Marcellus Shale	Shale	3097	1/1	
Middle Devonian		Onondaga	Limestone	3256	159 ,	
		Unconformity Interval		3285	29	
Upper Silurian		Salina - including Akron-Berite, Camillus, Syracuse, Vernon	Evaporites/Dolomite	3900	615	1781.
Upper Silurian		Lockport Dolomite	Dolomite	4108	208	
Lower Silurian	Clinton	Rochester Shale, Irondequoit-Reynales Dolomite	Sandstone	4260	122	
Lower Silurian		Medina, inlcuding the Grimsby and Whirlpool Sandstones	Sandstone/Shale	4439	179	

Notes



GEOLOGIC DATA BILLMAN GEOLOGIC CONSULTANTS REPORT

BILLMAN GEOLOGIC CONSULTANTS, INC.

TO:

MR KARL KIMMICH, LION ENERGY COMPANY, LLC

FROM:

DAN A. BILLMAN, PG, CPG, BILLMAN GEOLOGIC CONSULTANTS, INC.

SUBJECT:

GEOLOGIC REVIEW OF THE BITTINGER #2, PROPOSED SWD WELL

DATE:

04/05/2014

CC:

This memo is to be read in conjunction with the report entitled, "Geologic Review of the Bittinger Area, Planned SWD Site", dated 8/2/2010., Written by Dan A. Billman of Billman Geologic Consultants, Inc.

Billman Geologic Consultants, Inc. (BGC) was requested by Lion Energy Company, LLC to review the geology of a proposed SWD well at the Bittinger #2 (123-33944). The well is located in Columbus Township, Warren County, Pennsylvania. Specifically, the area is located in and around the Bittinger, Smith and Reed properties; collectively referred to as the "Bittinger SWD site". Figure 1 depicts the well base map of the Bittinger #2 area.

The Bittinger #2 (123-33944) was initially drilled by U.S. Energy Development and later acquired by Lion Energy, when Lion Energy acquired the field from Belden and Blake, Corp. The well was originally drilled to a total depth of 4,574′, into the Queenston Shale Formation. The well was naturally completed in the Medina Sandstone and Whirlpool Sandstone. The well had a natural reported open flow 554 mcf/d and a reported natural rock pressure of 1,100 psi, recorded after a buildup of 72 hours (refer to completion reports included as Appendix 1 of this memo).

Geologic Analysis of Data Associated with the Bittinger SWD Site

The initial report of the Bittinger SWD area discusses the geology of both the Medina Sandstone and Whirlpool Sandstone. The Bittinger #2 well is located approximately 1,200' west of the Bittinger #4 and located approximately 1,500' northeast of the Bittinger #1. After review of the logs and completion reports (Appendix 1) of the Bittinger #2, both the Medina (Grimsby) and Whirlpool Sandstones are similar to the correlative formations within the Bittinger #1 and Bittinger #4 wells.

BGC completed a review of the logs associated with the Bittinger #2 (123-33944), as well as the Bittinger #1 (123-33914), #4 (123-39874) and other wells in the immediate area (Table 1 of the original report). The Medina Sandstone (Grimsby Sandstone) has 38' of formation equal or greater than 6% porosity, while the average for the area was

39.2'. Likewise, The Whirlpool Sandstone has 12' of formation equal or greater than 6% porosity, while the average for the area was 11.1'. For both sandstone formations, the characteristics are very typical for the area.

In the Bittinger #2, there is approximately 625' between the top of the Medina (Grimsby) Sandstone and the top of the Upper Silurian Salina Formation. The Salina Formation is a series of evaporates (including salt and anhydrite), shale and carbonate formations, which based on lithology should have low permeability and have characteristics of a good confining interval. Given the ductile nature of the salt and anhydrite, natural fractures tend not to propagate vertically up to and through the Salina Formation. Also, between the Medina (Grimsby) Sandstone and the Salina Formation are other potential confining intervals, including the Vernon and Rochester Shales and the Packer Shell (Irondequoit and Reynales Dolomites). Another shale interval, the Power Glen Shale (occasionally referred to as the Cabot Head Shale) lies between the Medina (Grimsby) Sandstone and Whirlpool Sandstone.

Conclusions

The Bittinger #2 (123-33944) appears to have a very porous Whirlpool Sandstone interval to allow for saltwater injection and storage. The formation was naturally completed and therefore, it is assumed to have sufficient natural (unstimulated) porosity and permeability development. The Bittinger #2 SWD site is located in an area of minimal tectonic influence (i.e. folding and faulting of the rock), other than the gentle dip of the formation to the southeast (refer to mapping included in the original report). Given the nature of the Salina Formation (i.e. bedded salts and anhydrites) above the SWD interval, minimal through-going, vertical fractures are expected to exist in the Bittinger #2 SWD site area.

BGC has not verified ownership of Lion's properties or completed a site visit as part of the geologic review of the area.

Respectfully submitted by:

Dan A. Billman, PG, CPG

Dan a. Biller

President, Billman Geologic Consultants, Inc.

DISCLAIMER

This document includes forward-looking statements as well as historical information. Forward-looking statements include, but are not limited to statements relating to geological and seismic data interpretations, prospect reserve estimates and prospect risk. Although BGC believes that its expectations reflected in these forward-looking statements are reasonable, such statements involve risks and uncertainties, and no assurance can be given that actual results will be consistent with these forward-looking statements. Investment in oil and gas exploration is high risk by its very nature. Important factors that could cause actual results to differ from these forward-looking statements include, but are not limited to: erroneous interpretations of the seismic and geological data; the inability to acquire leases on identified prospects; mechanical problems while drilling and producing wells which prevent completion of a well or result in plugging of a well; dry holes; less reserves than originally estimated due to poor sand development or drainage by offsetting wells; non-commercial wells; and the variations in future gas pricing. BGC cannot and has not beyond normal due diligence care standards confirmed the accuracy and completeness of all the information we have reviewed in the course of this consulting engagement. Data for this review has been provided by Tetra Tech, NUS, Lion Energy, LLC or is publicly available and BGC, Inc. cannot be held responsible for errors in this provided data. Further, we express no opinion regarding any legal or securities issues. BGC shall assume no liability whatsoever for the use or reliance there upon by Tetra Tech, NUS, Lion Energy, LLC, their clients and/or their investors, of information, opinions and interpretations provided by BGC. BGC reserves the right to adjust these findings and interpretations with the discovery of relevant data or future production data.

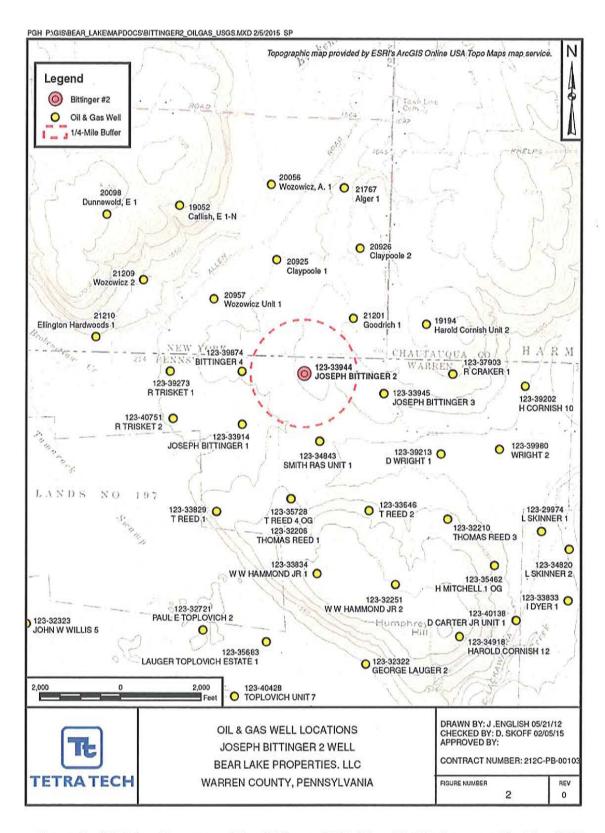
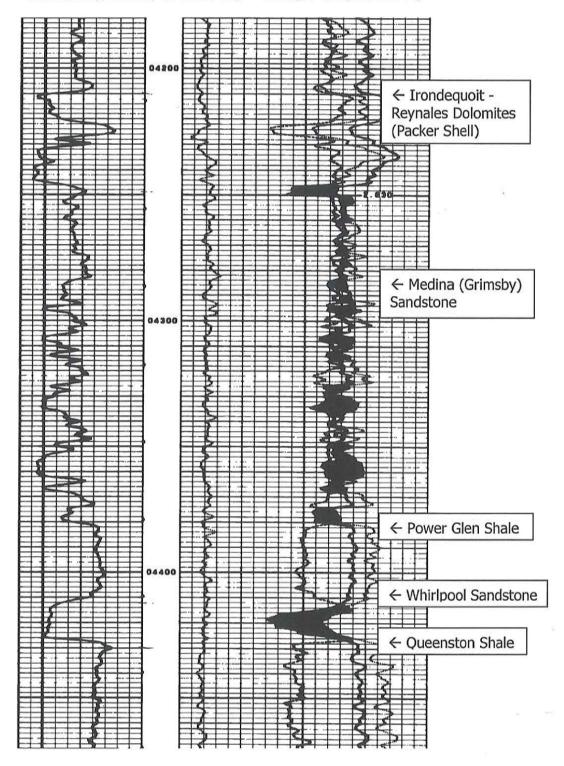


Figure 1: Well location map of the Bittinger SWD Site. Well being permitted for SWD Bittinger #2 (123-33944) centered in map.

Appendix 1:

Log Data and Completion Reports for the Bittinger #2 (123-33944)

Gamma Ray, Density Neutron Log -- Bittinger #2 (123-33944)



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Completion Report (page 2) -- Bittinger #2 (123-33944)

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BILLMAN GEOLOGIC CONSULTANTS, INC.

TO:

MR KARL KIMMICH, LION ENERGY COMPANY, LLC

FROM:

DAN A. BILLMAN, PG, CPG, BILLMAN GEOLOGIC CONSULTANTS, INC.

SUBJECT: GEOLOGIC REVIEW OF THE BITTINGER AREA, PLANNED SWD SITE

DATE:

08/02/2010

CC:

Billman Geologic Consultants, Inc. (BGC) was requested by Lion Energy Company, LLC to review the geology of a planned salt water disposal (SWD) site in Columbus Township, Warren County, Pennsylvania. Specifically, the area is located in and around the Bittinger, Smith and Reed properties; collectively referred to as the "Bittinger SWD site". Figure 1 depicts the wellbase map of the Bittinger SWD site area. The wells being permitted include the 123-33914 (Bittinger #1) and the 123-39874 (Bittinger #4).

Both the Bittinger #1 and Bittinger #4 were initially drilled by U.S. Energy Development and later acquired by Lion Energy, when Lion Energy acquired the field from Belden and Blake, Corp. In both the Bittinger #1 and Bittinger #4, the perforated and hydraulically fracture treated interval includes both the Lower Silurian Medina Sandstone and Lower Silurian Whirlpool Sandstone. These formations have been produced, commingled, since 1983 and 1987, respectfully (refer to completion reports, Appendix 1).

Geologic Analysis of Data Associated with the Bittinger SWD Site

BGC completed an analysis of the logs in the Bittinger SWD site area and the porosity per foot data is included in Table 1. Within the Whirlpool Sandstone, the Bittinger #1 (123-33914) encountered 10' of sand greater or equal to 6% (log measured) porosity and 8' of sand greater or equal to 10% (log measured) porosity. Within the Medina Sandstone, the Bittinger #1 (123-33914) encountered 23' of sand greater or equal to 6% (log measured) porosity and 0' of sand greater or equal to 10% (log measured) porosity. Within the Whirlpool Sandstone, the Bittinger #4 (123-39874) encountered 11' of sand greater or equal to 6% (log measured) porosity and 7' of sand greater or equal to 10% (log measured) porosity. Within the Medina Sandstone, the Bittinger #4 (123-39874) encountered 38' of sand greater or equal to 6% (log measured) porosity and 0' of sand greater or equal to 10% (log measured) porosity.

The Whirlpool Sandstone across the producing Medina/Whirlpool trend is interpreted as a bar sand system and where it is present, it is often been a prolific hydrocarbon producer. Initial analysis of the Bittinger SWD site data indicates that the Whirlpool

Sandstone is a consistently porous formation with a significant footage of porosity greater than 10% porosity. Gamma Ray, Density Neutron logs of the Medina/Whirlpool section of the Bittinger #1 and Bittinger #4 are included in Appendix 1. The Bittinger #1 has a peak, logged porosity of approximately 16% and the Bittinger #4 has a peak, logged porosity of approximately 18%. Cross-sections, oriented along regional strike (southwest – northeast) and regional dip (northwest – southeast) were constructed across the Bittinger SWD site and are included as an attachment to this report. The consistency of thickness and porosity of the Whirlpool Sandstone is evident in the cross-sections (Appendix 2).

The Medina Sandstone is interpreted as a braided channel system and therefore porous, reservoir quality Medina Sandstone typically is a very discontinuous across even short distances. As expected, within the logs of the Bittinger #1 and Bittinger #4 (Appendix 1) the Medina Sandstone is a series of interbedded sandstones, silts and shales and has a discontinuous nature from well to well. In the Bittinger #1 and Bittinger #4, porosities average 8% and lower, from sand body to sand body within the Medina interval in each well.

Both the Whirlpool and Medina Sandstones were mapped using footage at 8% porosity or greater cut-off. These maps are included, with this report, as Appendix 2.

Figure 2 depicts the structure on top of the Packer Shell (dolomites above the Medina Formation) in the Bittinger SWD site area. The structural mapping shows a very consistently dipping formation from the northeast to the southwest across the Bittinger SWD site. No obvious faulting or "deviations" from regional dip are evident on the structural top of the Packer Shell dolomites. Figure 3 depicts the structure on top of the Queenston Shale (Base of the Whirlpool Sandstone) in the Bittinger SWD site area. The structural mapping shows a very consistently dipping formation from the northeast to the southwest across the Bittinger SWD site. No obvious faulting or "deviations" from regional dip are evident on the structural top of the Queenston Shale. Both formations appear to show a fairly tectonically inactive situation exists in the Medina/Whirlpool interval at the Bittinger SWD site.

Approximately 850' above the top of the Medina Sandstone is the top of the Upper Silurian Salina Formation, a series of evaporates (including salt and anhydrite), shale and carbonate formations. The top of the Salina Salt (the evaporites within the Salina Formation) occurs approximately 650' above the top of the Medina Sandstone. Given the ductile nature of the salt and anhydrite, natural fractures tend not to propagate vertically up to and through the Salina Formation.

Conclusions

The Bittinger #1 and Bittinger #4 appear to have a very porous Whirlpool Sandstone interval to allow for saltwater injection and storage and was previously hydraulic fractured, allowing for increased permeability. The Bittinger SWD site is located in an area of minimal tectonic influence (i.e. folding and faulting of the rock), other than the gentle dip of the formation to the southeast (mapping included in Appendix 2). Given the nature of the Salina Formation above the SWD interval, minimal through-going, vertical fractures are expected to exist in the Bittinger SWD site area.

As a disclaimer, BGC has not had access to seismic data in and around the Bittinger SWD site and any observations or conclusions made are not made with the knowledge of seismic data. BGC has not verified ownership of Lion's properties or completed a site visit as part of the geologic review of the area.

Respectfully submitted by:

Dan A. Billman, PG, CPG

Dan a. Billion

President, Billman Geologic Consultants, Inc.

DISCLAIMER

This document includes forward-looking statements as well as historical information. Forward-looking statements include, but are not limited to statements relating to geological and seismic data interpretations, prospect reserve estimates and prospect risk. Although BGC believes that its expectations reflected in these forward-looking statements are reasonable, such statements involve risks and uncertainties, and no assurance can be given that actual results will be consistent with these forward-looking statements. Investment in oil and gas exploration is high risk by its very nature. Important factors that could cause actual results to differ from these forward-looking statements include, but are not limited to: erroneous interpretations of the seismic and geological data; the Inability to acquire leases on identified prospects; mechanical problems while drilling and producing wells which prevent completion of a well or result in plugging of a well; dry holes; less reserves than originally estimated due to poor sand development or drainage by offsetting wells; non-commercial wells; and the variations in future gas pricing. BGC cannot and has not beyond normal due diligence care standards confirmed the accuracy and completeness of all the information we have reviewed in the course of this consulting engagement. Data for this review has been provided by Lion Energy, LLC or is publicly available and BGC, Inc. cannot be held responsible for errors in this provided data. Further, we express no opinion regarding any legal or securities issues. BGC shall assume no liability whatsoever for the use or reliance there upon by Lion Energy, LLC, their clients and/or their investors, of information, opinions and interpretations provided by BGC. BGC reserves the right to adjust these findings and interpretations with the discovery of relevant data or future production data.

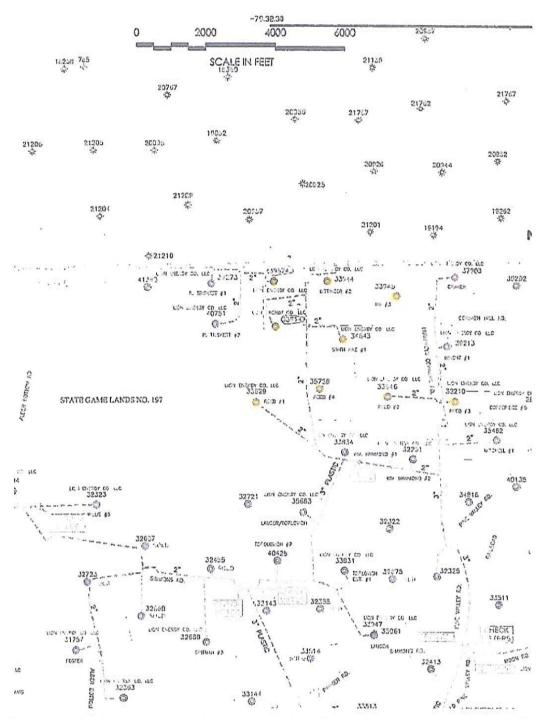


Figure 1: Well location map of the Bittinger SWD Site. Wells being permitted for SWD include the 123-33914 (Bittinger #1) and the 123-39874 (Bittinger #4).

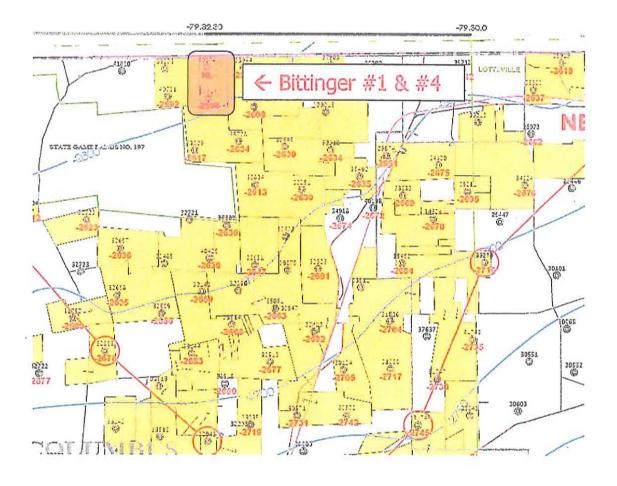


Figure 2: Map of the structure on top of the Packer Shell (above the Medina Sandstone). Structure on top of the Packer Shell is very consistently dipping to the southeast. The 123-33914 (Bittinger #1) and the 123-39874 (Bittinger #4) highlighted in orange.

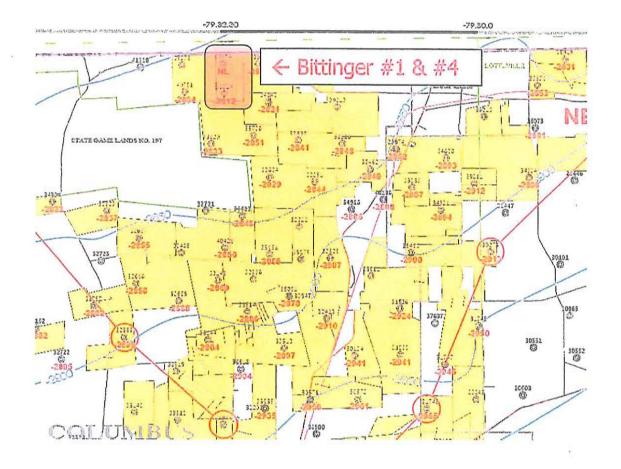


Figure 3: Map of the structure on top of the Queenston Shale (base of the Whirlpool Sandstone). Structure on top of the Queenston Shale is very consistently dipping to the southeast. The 123-33914 (Bittinger #1) and the 123-39874 (Bittinger #4) highlighted in orange.

Table 1: Log Data from Wells in the Area of Study

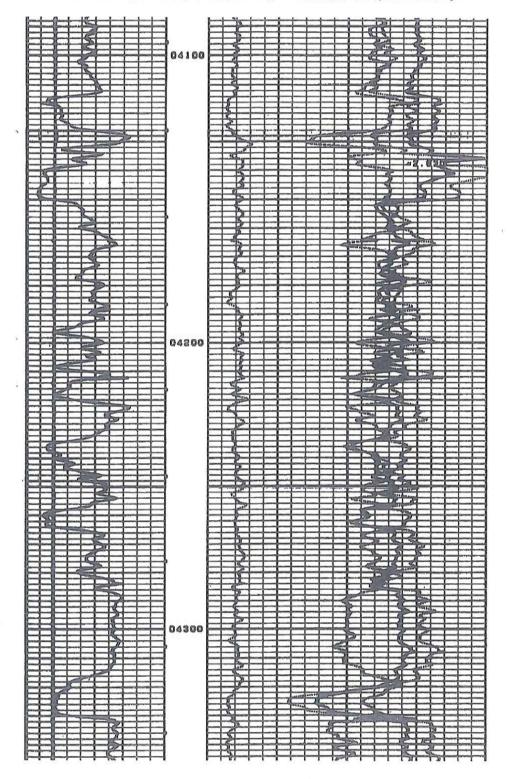
API#	Whirlpool 6%	Whirlpool 8%	Whirlpool 8% Whirlpool 10% Medina 6% Medina 8% Medina 10%	Medina 6%	Medina 8%	Medina 10%
123-33914	10	6	8	23	6	0
123-33944	12	10	6	38	7	0
123-33945	13	11	8	54	6	0
123-39874	11	10	7	38	9	0
123-34843	12	10	7	25	2	0
123-33829	11	9	8	42	7	0
123-35728	14	12	11	57	33	10
123-33646	8	5	3	47	10	1
123-32210	6	7	4	29	3	0
Average:	11.1		Average:	39.7		

7

Appendix 1:

Log Data and Completion Reports for the Wells Being Permitted as Salt Water Disposal Wells

Gamma Ray, Density Neutron Log -- Bittinger #1 (123-33914)



Completion Report (page 1) -- Bittinger #1 (123-33914)

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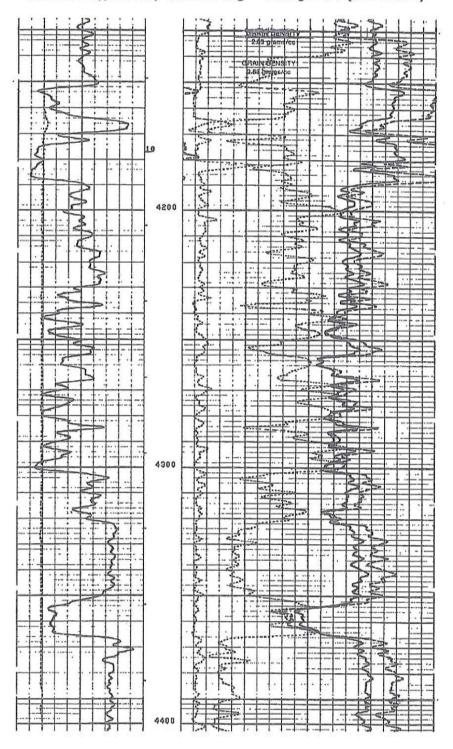
Completion Report (page 2) -- Bittinger #1 (123-33914)

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Hamilton Shales	2785	2955'				
Onondaga	29551	3129'				
Unconformity Interval	3129'	3145'				
Akron-Bertie	3145	3220'			Salt @ 3935'	1
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Syracuse	3298	3525'				
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Gamma Ray, Density Neutron Log -- Bittinger #4 (123-39874)



Completion Report (page 1) -- Bittinger #4 (123-39874)

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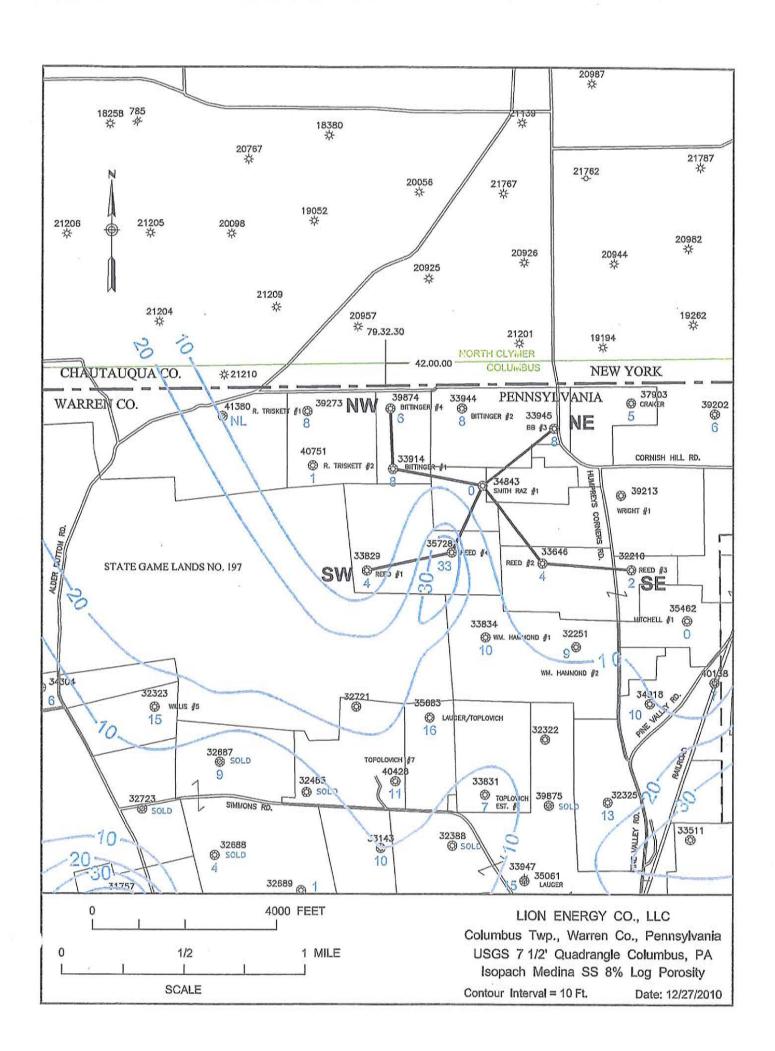
Completion Report (page 2) -- Bittinger #4 (123-39874)

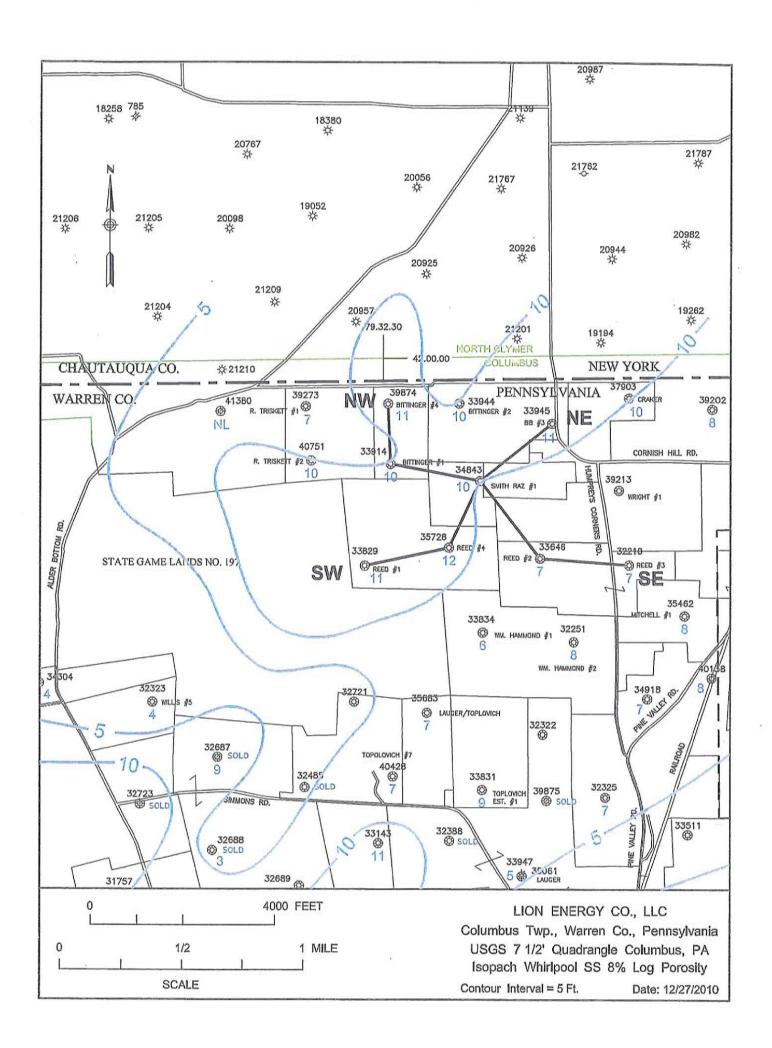
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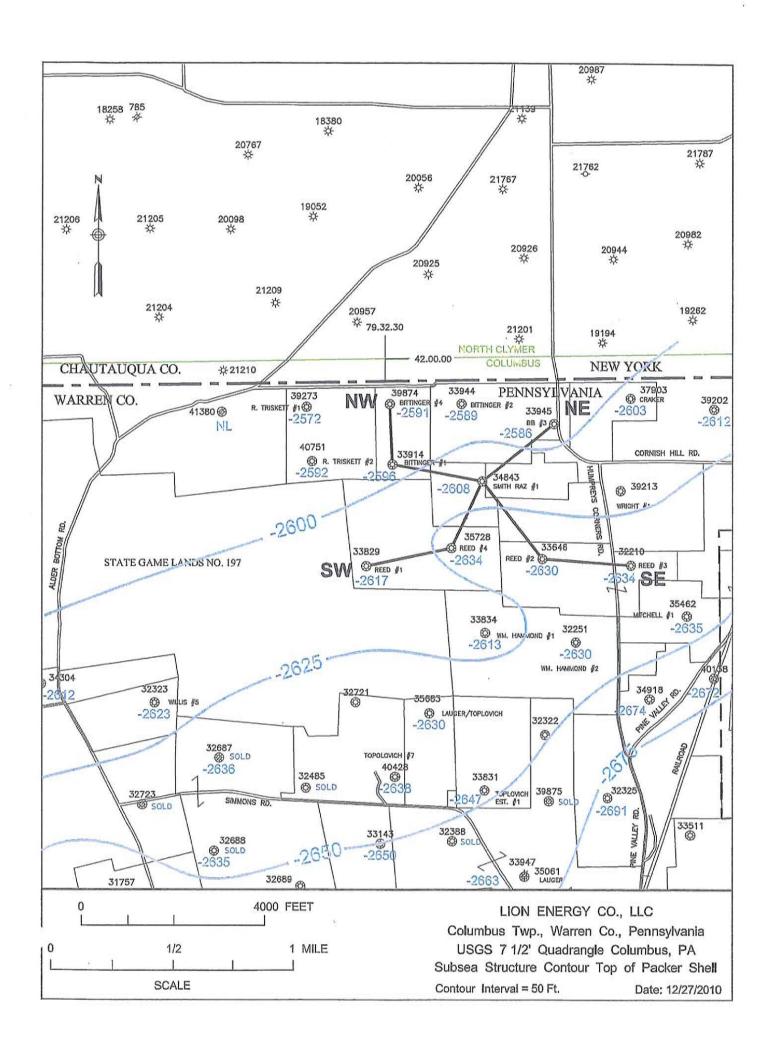
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Camillus	3292'	3366'				1
Syracuse	3366'	3547'			1	1
Sa1t	3547'	3896'				
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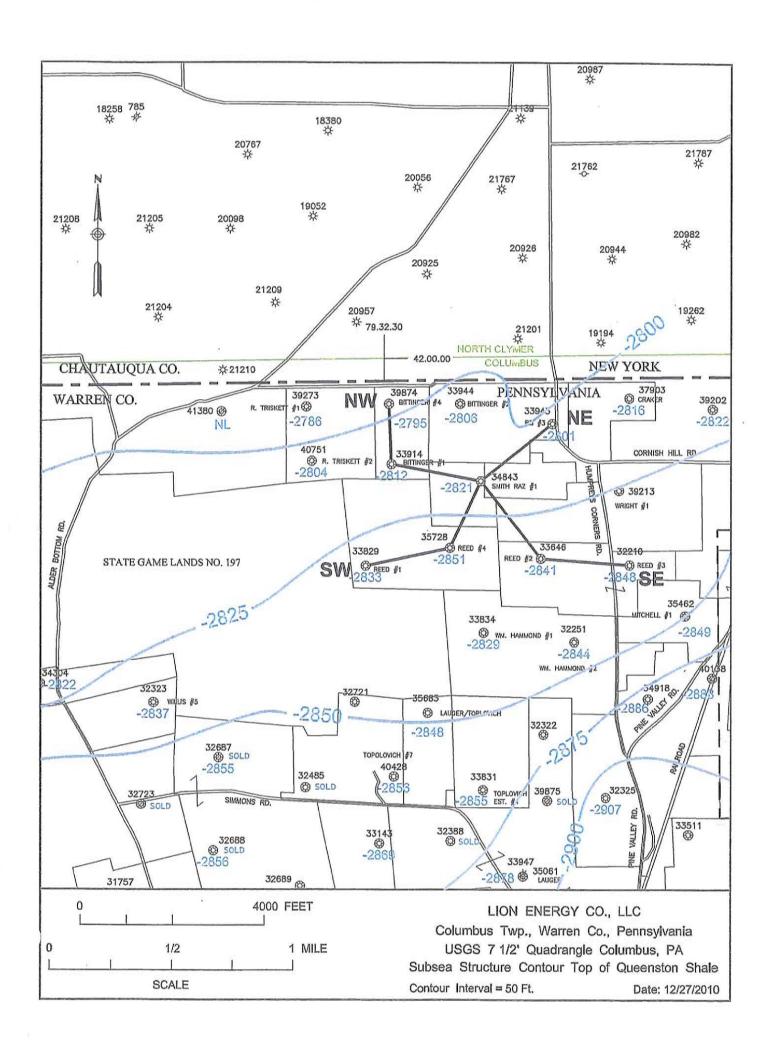
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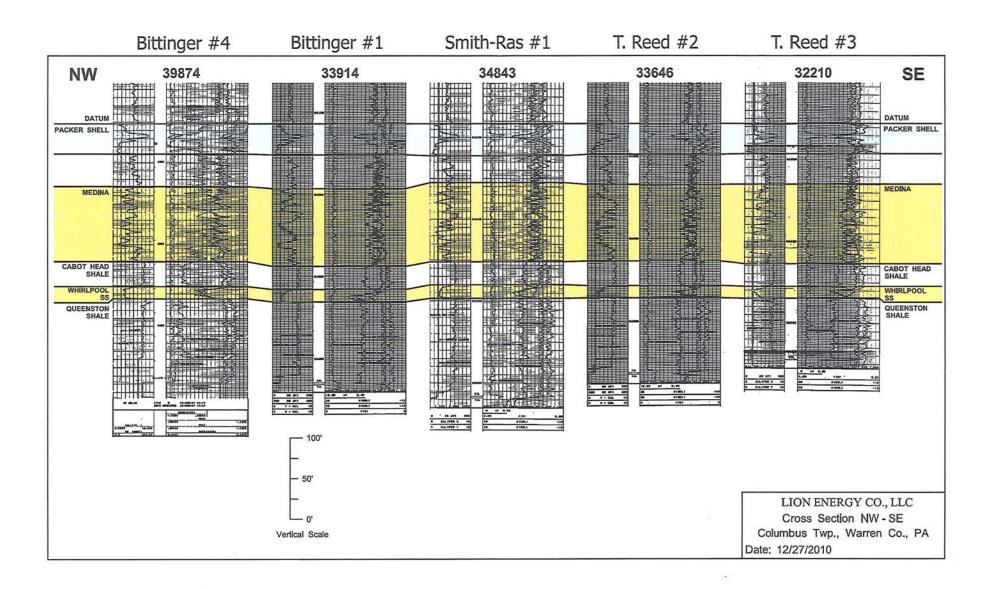
Cross-sections, Isopach and Structural Mapping Bittinger SWD Site

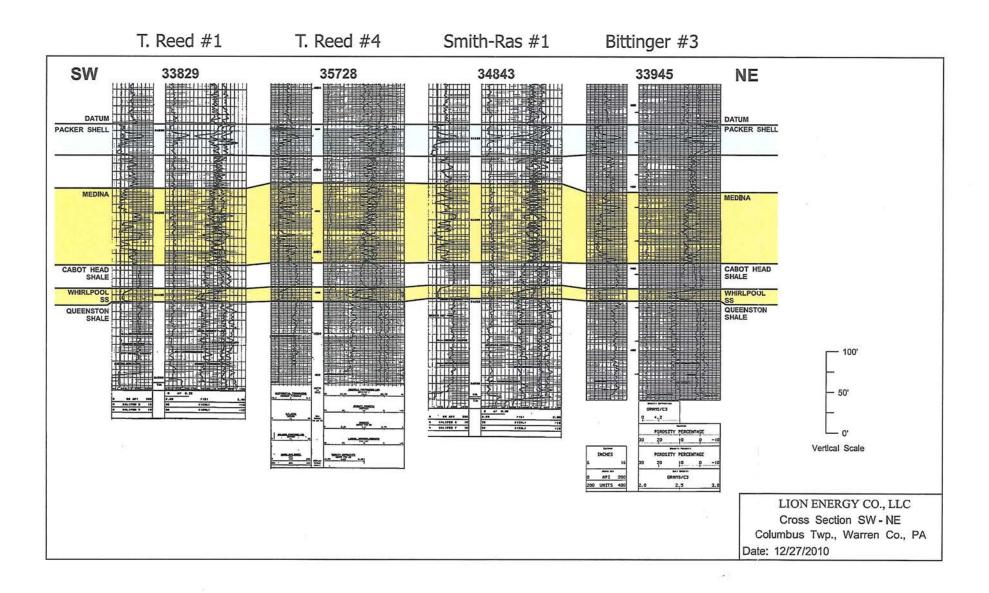












GEOLOGIC DATA BITTINGER #3 COMPLETION RECORD

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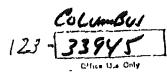
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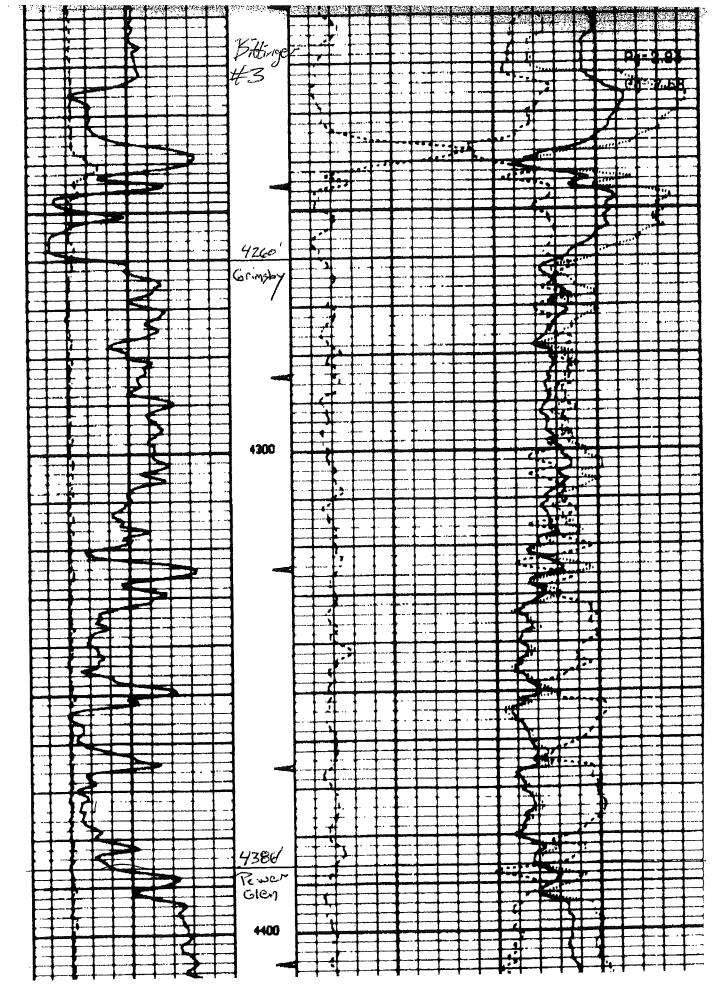
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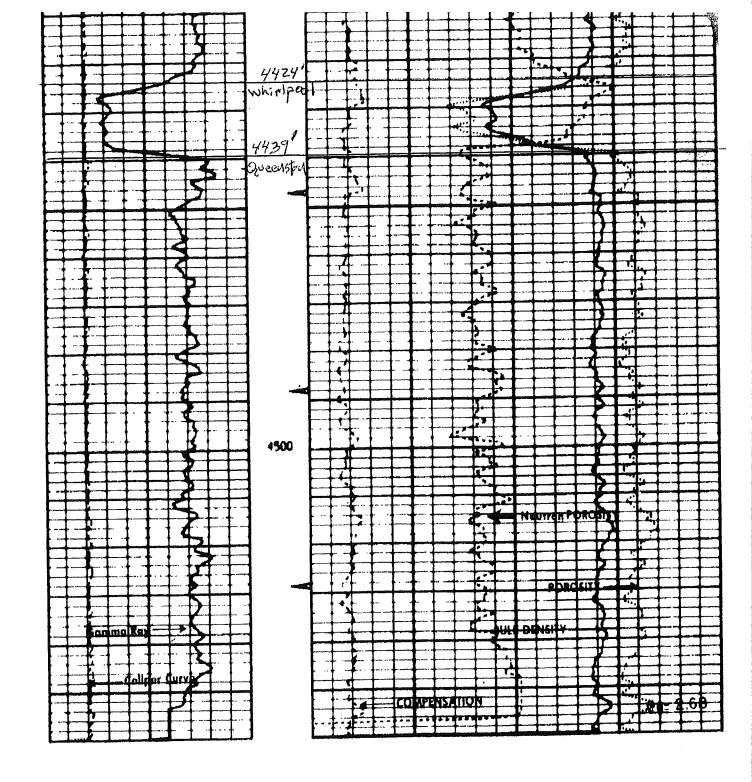
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GEOLOGIC DATA MAXIMUM INJECTION PRESSURE CALCULATIONS

Maximum Injection Pressure (MIP) Calculations for Bear Lake Properties Bittinger #3 Well

Warren County, PA

1) Frac Gradient (FG) Based on Nearby Smith- Ras #1 Well

 $FG = [ISIP + (.433 \times SG \times D)] /D$

Where:

ISIP = 2200 psi

SG = 1.0 (frac fluid)

D = 4391

					Fracture
		Hydrostatic			Gradient
Well	ISIP (psi)	Factor (psi/ft)	SG	D (ft)	(psi/ft)
Smith/Ras #1	2200	0.433	1	4391	0.934

2) Maximum Injection Pressure (MIP) Calculation for Bittinger #3 Well Using FG from Smith-Ras #1 Frac

 $MIP = [FG - (.433XSG)] \times D$

FG = 0.934

SG = 1.218 (brine)

Depth:

Medina Top

4260

					Fracture	
		Hydrostatic			Gradient	MIP
		Factor (psi/ft)	SG	D (ft)	(psi/ft)	(Surface)
Bittinger #3	-	0.433	1.218	4260	0.934	1732

GEOLOGIC DATA SMITH - RAS #1 WELL DATA

ER-OG-4; Rev. 2/80 COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL RESOURCES DIVISION OF OIL AND GAS REGULATION PITTSBURGH, PENNSYLVANIA 15222 WELL RECORD

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RERM	WAR	-34843	PROJECT NO.		TYPE OF W	ELL Gas	
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WELL OF	PERATOR		Bergerade equipos	J. Frankly,	TELEPHONE NO.	1	
	II describerto U.S.	Energy Developm	ment Corporation		anger with the second management and the second	(716)856-	
ADDRES	670	Statier Building	Buffalo, NY		h waste	In chart Zip	14202
FARM N	AMERICA	T tosu		FARM NO.	SERIAL NO.		ACRES
	Smit		COUNTY	#1		17 - 28 - 37 - 1	72
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	ON:	V 1 1 11 11	QUADRANGLE		₩ 7%!		 .
	1575		Columbus		, au	4	
		1	CASING AND TUBING	RECORD	pitalis sama and a sam	T	
PIPE SIZE	AMOUNT IN	MATERIAL CEMENT (SKS)	PEHIND PIPE		KER	1	DATE
	 		GEL (SKS.)	1	SIZE	DEPTH	
8 5/8!!	406	150	A CONTRACTOR OF THE PARTY OF TH			41501	3/22/84
4 1/2!!	4493		150	Concrete of	neparkritien -		-3/26/84
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	INTERVAL	PERFORATED		INTERVAL	AMOUNT	AMOUNT	
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/27/84	4269 10%		6/27/84	4269-	674 bbls	58:000#	 21 RPM
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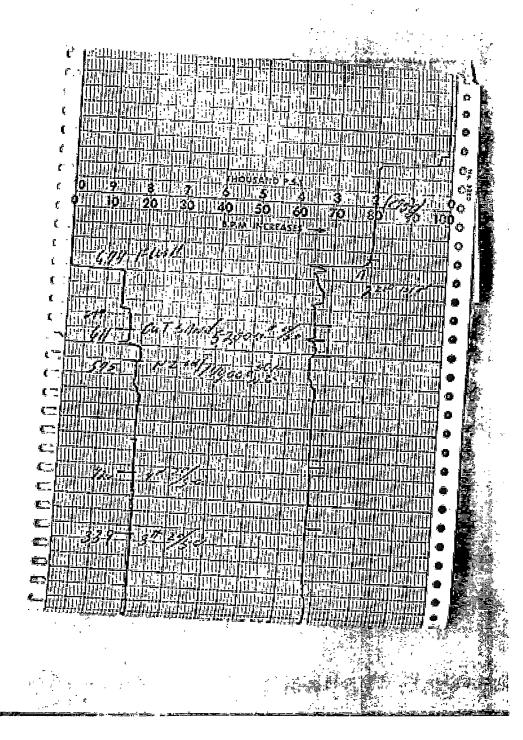
		FORM	RATIONS			
NAME	тоғ	BOTTOM	GAS AT	OIL AT	WATER AT (FRESH OR SALT WATER)	SOURCE OF
Unconsolidated Gravel	. 0.	120'			Fresh @ 105'	Drillers
Devonian Shale	120'	2768'				records geophysic
"Tully" Limestone	2768	2877'				logs
Hamilton Shales	2877 '	ا 3049				
Onondaga	30491	3218'				
Unconformity Interval	3218'	3233'				
Akron-Bertie	3233'	3317'				
Camillus	33171	33891				
Syracuse	33891	3597 '				
Vernon	35971	3861'				
Salt Zone	3579'	3785 '				
Lockport	3861'	4065 '			Salt @ 3910'	
Rochester	4065 '	4184'				
Irondequoit-Reynales	4184	42221				
Grimsby	42221	4351'				
Power Glen	43511	4383'				
∜hirlpool	4383	43961		٠.	i	
Queenston	4396	TD				
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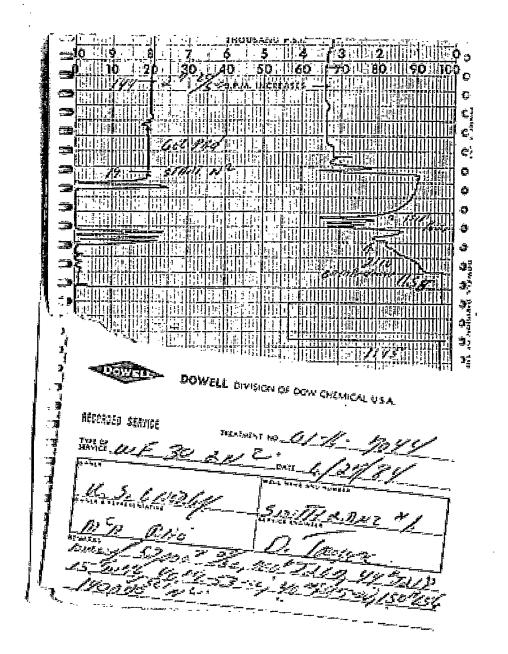
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July 17	. 1984
DATE	
Dong Pan K Wall	
APPROVED BY	
Douglas K. Walch, Geophysicist	

Well Name & No	/RAS #1	Loc		
Permit No.		Twp.,	WIRPFN	Co+, gasala
restantante		ION RECORD		
Company 1 1 McGelloush _	Formation	Madia s (Chietana)	l Date	1774,184
Pumped in 500 gol. ocid	and 5(X) gel. We	ter, ran Ges	na Ray and a	collar log.
PHTD CART IT. FOIL B	Z TOTTOMS"			
4279 - 4316 W/	shots -	4987	4391_W/_	shots
4305 4918 W/	នាក្រាះត =	<u>, ሊባው</u>	- ^{7,7}	
4136 w/	shots -	4391 -		shots
Size of shots	.42	Te	etal Shots _	ាព័
	FRAC J	IOB	M-l-	6/27/84
Company Baveli Schlembers	žΤ			
Loaded hole. Broke form	ation @_?180_# E	Sack to <u>950</u>	e terrest sic fr transfer	follows:
152 KCL _ Acid 0 _n _B			LE TIMPER SS	* ***
men e lesse	# Per	SAND Size	DPM	Press.
BBLS./EEL.	Gal.	and the standard		•
1. 0-199	PAR	يب مد مد <u>مو</u> ندم مد مد مو	974	3500
2. 144-335	20	20/50	21	- 3350)
3. <u>930-420</u>	39	20/50	21	3250
4, 470-411	<u>L</u> ŧ	20/50	20)	3500
5. <u>611-673</u>	Flush	2 B	14.5	3500
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ISIP 2200 P	5"MIN.	1950	Job comp	lete <u>12:36 P</u> .
Open to pit 1:26 PM	Flowed back 24_	hra. Total	water <u>675</u>	bbls.
52,000 # 20/68 A HHP used 1734 . Ni				
REMARKS: As \$40 BBLS cut			KSES eut sand	្ត់ ៥៤០ ខុស ២៩៤៣
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pressure - well servoused	gr: = 4 x5L7 50000 (ter a reissie en (16)	127	
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XII.				TWATLE 114 (24),

7-6-84





GEOLOGIC DATA MEDINA GAS PRODUCTION SUMMARY

Permit	Company	Year		Quantity (MCF)	Brine	Days	County	Municipality	Farm_Name	Farm_Well_No	Field	Pool	Completion Date
123-33944	US ENERGY DEV CORP	1984	GAS	5,812		0	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1985	GAS	22,275		0	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1986	GAS	30,101		336	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1987	GAS	23,479		336	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1988	GAS	47,976		347	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1989	GAS	50,332		352	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1990	GAS	39,609		346	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1991	GAS	21,121		347	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1992	GAS	6,351		323	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1993	GAS	3,039		339	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1994	BRINE		22		WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	US ENERGY DEV CORP	1994	GAS	1,402		319	WARREN	COLUMBUS	JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
123-33944	BELDEN & BLAKE CORP	2000	GAS	698		366			JOSEPH BITTINGER	2	COLUMBUS	DEWEY CORNERS	29-Jan-84
	BELDEN & BLAKE CORP	2001	GAS	67		365	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	BELDEN & BLAKE CORP	2002	GAS	0		0	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	BELDEN & BLAKE CORP	2002	OIL	0		0		COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	RANGE RESOURCES APPALACHIA LLC	2002	GAS	5		31	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	RANGE RESOURCES APPALACHIA LLC	2003	GAS	701		334		COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	RANGE RESOURCES APPALACHIA LLC	2004	GAS	718		365	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	RANGE RESOURCES APPALACHIA LLC	2005	GAS	670		334	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	RANGE RESOURCES APPALACHIA LLC	2006	GAS	374		334	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	TRINITY ENERGY CORP	2007	GAS	102		122	WARREN	COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	LION ENERGY CO LLC	2008	GAS	193		365		COLUMBUS	JOSEPH BITTINGER	2		DEWEY CORNERS	29-Jan-84
	LION ENERGY CO LLC	2009	GAS	30		30		COLUMBUS		2		DEWEY CORNERS	29-Jan-84
125-55544	LION ENERGY CO ELC	2003	Total	255,055	22	30	WARREN	COLOIVIBOS	JOSEPH BITTINGER	2	COLUMBOS	DEVVET CORNERS	23-1411-04
			Total	255,055	22								
Permit	Company	Year	Product	Quantity		Dave	County	Municipality	Farm_Name	Farm_Well_No	Field	Pool	Completion Date
	US ENERGY DEV CORP	1986	GAS	32,248		336	TOTAL PROPERTY.	Parade and the second	JOSEPH BITTINGER	3	The state of the s	DEWEY CORNERS	19-Oct-84
	US ENERGY DEV CORP	1987	GAS	36,330		336	WARREN	COLUMBUS	JOSEPH BITTINGER	3	COLUMBUS		19-Oct-84
	US ENERGY DEV CORP	1988	GAS	48,995		345	WARREN	COLUMBUS	JOSEPH BITTINGER	3		DEWEY CORNERS	19-Oct-84
				40,000			AAWINITIA	COLONIDOS	JOSEPH BITTINGER			DEWEL COMMENS	13-001-04
123-333-43		1020	GAS	42 806			MARREN	COLLIMBUS	IOSEDH BITTINGER	2		DEWLEY CORNERS	10 Oct 94
	US ENERGY DEV CORP	1989	GAS	42,806		332	WARREN	COLUMBUS	JOSEPH BITTINGER	3	COLUMBUS	DEWEY CORNERS	19-Oct-84
123-33945	US ENERGY DEV CORP US ENERGY DEV CORP	1990	GAS	26,642		332 343	WARREN	COLUMBUS	JOSEPH BITTINGER	3	COLUMBUS COLUMBUS	DEWEY CORNERS	19-Oct-84
123-33945 123-33945	US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP	1990 1991	GAS GAS	26,642 13,848		332 343 347	WARREN WARREN	COLUMBUS COLUMBUS	JOSEPH BITTINGER JOSEPH BITTINGER	3 3	COLUMBUS COLUMBUS COLUMBUS	DEWEY CORNERS DEWEY CORNERS	19-Oct-84 19-Oct-84
123-33945 123-33945 123-33945	US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP	1990 1991 1992	GAS GAS GAS	26,642 13,848 5,278		332 343 347 315	WARREN WARREN WARREN	COLUMBUS COLUMBUS COLUMBUS	JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER	3 3 3	COLUMBUS COLUMBUS COLUMBUS	DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS	19-Oct-84 19-Oct-84 19-Oct-84
123-33945 123-33945 123-33945 123-33945	US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP	1990 1991 1992 1993	GAS GAS GAS GAS	26,642 13,848	72	332 343 347	WARREN WARREN WARREN WARREN	COLUMBUS COLUMBUS COLUMBUS	JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER	3 3 3	COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS	DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS	19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84
123-33945 123-33945 123-33945 123-33945 123-33945	US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP	1990 1991 1992 1993 1994	GAS GAS GAS GAS BRINE	26,642 13,848 5,278 4,826	73	332 343 347 315 360	WARREN WARREN WARREN WARREN WARREN	COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS	JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER	3 3 3 3	COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS	DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS	19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84
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123-33945 123-33945 123-33945 123-33945 123-33945 123-33945 123-33945	US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP BELDEN & BLAKE CORP	1990 1991 1992 1993 1994 1994 2001	GAS GAS GAS GAS BRINE GAS GAS	26,642 13,848 5,278 4,826 1,810 66	73	332 343 347 315 360 363 365	WARREN WARREN WARREN WARREN WARREN WARREN	COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS	JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER	3 3 3 3 3 3	COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS	DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS	19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84
123-33945 123-33945 123-33945 123-33945 123-33945 123-33945 123-33945	US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP US ENERGY DEV CORP BELDEN & BLAKE CORP BELDEN & BLAKE CORP	1990 1991 1992 1993 1994 1994 2001 2002	GAS GAS GAS BRINE GAS GAS	26,642 13,848 5,278 4,826 1,810 66 40	73	332 343 347 315 360 363 365 365	WARREN WARREN WARREN WARREN WARREN WARREN WARREN WARREN	COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS	JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER JOSEPH BITTINGER	3 3 3 3 3 3 3 3 3	COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS COLUMBUS	DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS DEWEY CORNERS	19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84 19-Oct-84
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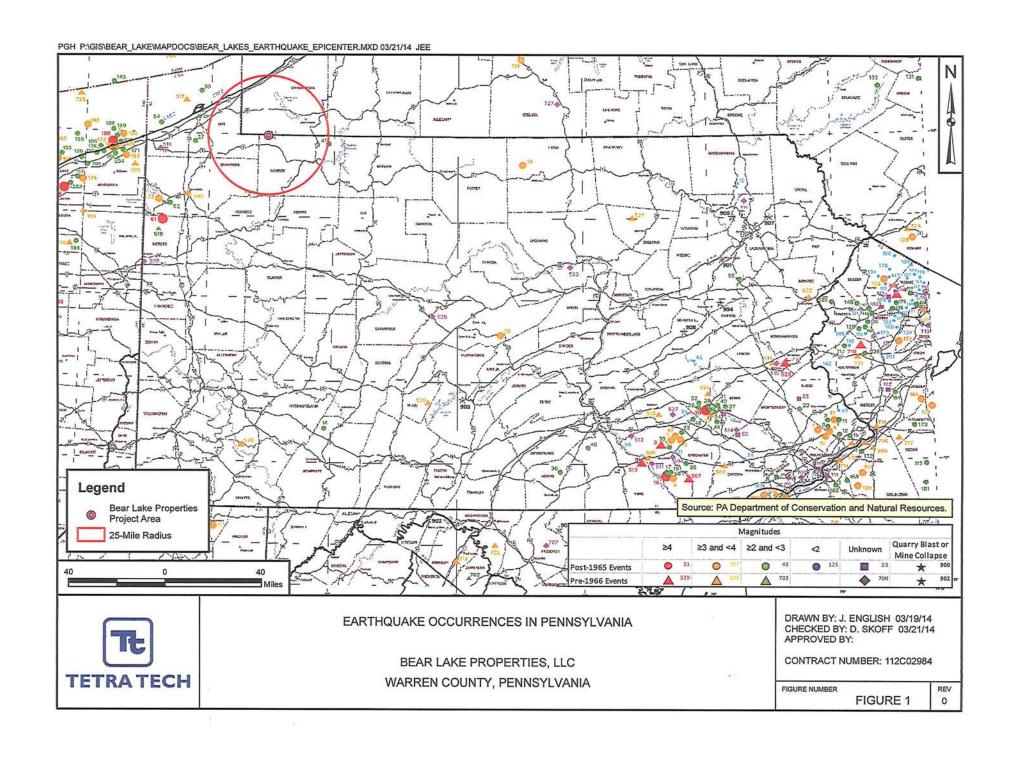
123-39273 US ENERGY DEV CORP	1986	GAS	29,581		308	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	1987	GAS	26,012		322	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	1988	GAS	34,866		307	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	1989	GAS	60,104		352	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	1990	GAS	29,211		335	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	1991	GAS	6,338		293	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	1992	GAS	3,309		321	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	1993	GAS	1,474		165	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	2000	GAS	519		240	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP	2001	GAS	1,166		365	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 BELDEN & BLAKE CORP	2001	GAS	15		365	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP		GAS	684		365	WARREN	COLUMBUS	R TRISKET	1	COLUMBUS	DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP		GAS	527		365		COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP		GAS	1,073		365		COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP		GAS	1,485		365		COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP		BRINE	1,405	5	505		COLUMBUS	R TRISKET	ī		DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP		GAS	1,068	-	365		COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP		BRINE	1,000	5	505		COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
123-39273 US ENERGY DEV CORP		GAS	398	3	240		COLUMBUS	R TRISKET	ī		DEWEY CORNERS	14-Dec-84
123-39273 LION ENERGY CO LLC		GAS	201		365		COLUMBUS	R TRISKET	1		DEWEY CORNERS	14-Dec-84
123-39273 LION ENERGY CO LLC		GAS	596		365		COLUMBUS	R TRISKET	1		DEWEY CORNERS	
125-39275 LION ENERGY COLLC		Total	222,127	10	303	WARREIN	COLOIVIBOS	K I KISKET	*:	COLUMBOS	DEWEI CORNERS	14-060-04
		Total	222,121	10								
Permit Company	Year	Product	Quantity		Days	County	Municipality	Farm_Name	Farm Well No	Field	Pool	Completion Date
123-39874 US ENERGY DEV CORP		GAS	11,653		112	THE PROPERTY OF	COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 US ENERGY DEV CORP		GAS	100,800		352		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 US ENERGY DEV CORP		GAS	100,330		355		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 US ENERGY DEV CORP		GAS	60,844		342		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
		GAS	35,401		324		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 US ENERGY DEV CORP		GAS	13,041		315		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87 20-Aug-87
123-39874 US ENERGY DEV CORP		GAS	하면 아이에 하네				COLUMBUS		4		DEWEY CORNERS	1000 - 100 - 100 m
123-39874 US ENERGY DEV CORP		BRINE	6,946	137	360		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 US ENERGY DEV CORP			r 770	13/	264		: TAN TAN TAN TAN	BITTINGER	35			20-Aug-87
123-39874 US ENERGY DEV CORP		GAS	5,778		361		COLUMBUS	BITTINGER	4	COLUMBUS		20-Aug-87
123-39874 BELDEN & BLAKE CORP		GAS	92		365		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 BELDEN & BLAKE CORP		GAS	21		365		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 BELDEN & BLAKE CORP		GAS	551		273		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 BELDEN & BLAKE CORP		OIL	0		0		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 RANGE RESOURCES APPALACHIA LLC		GAS	5		62		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 RANGE RESOURCES APPALACHIA LLC		GAS	79		242		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 RANGE RESOURCES APPALACHIA LLC		GAS	308		214		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 TRINITY ENERGY CORP		GAS	32		122		COLUMBUS	BITTINGER	4		DEWEY CORNERS	20-Aug-87
123-39874 LION ENERGY CO LLC		BRINE		38			COLUMBUS	BITTINGER	4	COLUMBUS		20-Aug-87
123-39874 LION ENERGY CO LLC		GAS	388		365		COLUMBUS	BITTINGER	4	COLUMBUS		20-Aug-87
123-39874 LION ENERGY CO LLC	2009	GAS	219		180	WARREN	COLUMBUS	BITTINGER	4	COLUMBUS	DEWEY CORNERS	20-Aug-87
		Total	336,487	175								
where we want to the second	September 1		***************************************					WEDGERSON & WESTCHER	WOODS AND AND	Ter er		ACCOUNT OF STREET
Permit Company			Quantity			County		Farm_Name	Farm_Well_No	Field	Pool	Completion Date
123-40751 US ENERGY EXPLORATION CORP		GAS	41,981		315	WARREN		R. TRISKET	2	COLUMBUS		5-Jan-90
123-40751 US ENERGY DEV CORP		GAS	47,292		357		COLUMBUS	R. TRISKET	2	COLUMBUS		5-Jan-90
123-40751 US ENERGY DEV CORP		GAS	25,943		322		COLUMBUS	R. TRISKET	2		DEWEY CORNERS	5-Jan-90
123-40751 US ENERGY DEV CORP	1993	GAS	17,584		359	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90

123-40751 US ENERGY DEV CORP	1994	BRINE		137		WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 US ENERGY DEV CORP	1994	GAS	19,177		363	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2000	BRINE		5		WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2000	GAS	5,514		366	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2001	BRINE		17		WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2001	GAS	4,531		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2002	GAS	2,340		273	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 BELDEN & BLAKE CORP	2002	OIL	0		0	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2002	GAS	205		31	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2003	BRINE		45	365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2003	GAS	1,594		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2004	GAS	1,422		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2005	GAS	1,554		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 RANGE RESOURCES APPALACHIA LLC	2006	GAS	1,414		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 TRINITY ENERGY CORP	2007	GAS	278		122	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 LION ENERGY CO LLC	2008	GAS	869		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
123-40751 LION ENERGY CO LLC	2009	GAS	1,506		365	WARREN	COLUMBUS	R. TRISKET	2	COLUMBUS	DEWEY CORNERS	5-Jan-90
		Total	173,205	204								
Permit Company	Year	Product	Quantity		Days	County	Municipality	Farm_Name	Farm_Well_No	Field	Pool	Completion Date
123-34843 US ENERGY DEV CORP	1985	GAS	17,683		0	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1986	GAS	31,402		336	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1987	GAS	29,357		322	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1988	GAS	50,639		338	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1989	GAS	52,016		344	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1990	GAS	21,148		330		COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1991	GAS	8,423		327	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1992	GAS	1,513		291	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1993	GAS	2,088		268	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 US ENERGY DEV CORP	1994	GAS	1,781		363	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 LION ENERGY CO LLC	2008	GAS	270		365	WARREN	COLUMBUS	SMITH- RAS	1 .	COLUMBUS	DEWEY CORNERS	26-Mar-84
123-34843 LION ENERGY CO LLC	2009	GAS	644		365	WARREN	COLUMBUS	SMITH- RAS	1	COLUMBUS	DEWEY CORNERS	26-Mar-84
		Total	216,965									
122 22014 HC ENERGY DEV CORD	1004	CAC	F802		•	MARREN	COLLINADUIC	IOCEDII DITTINGED	7	COLLINABLIC	DELL'EV CODMEDO	20.0
123-33914 US ENERGY DEV CORP	1984 1985	GAS GAS	5893		0		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1985	GAS	14431.49 44172.28		336		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	
123-33914 US ENERGY DEV CORP 123-33914 US ENERGY DEV CORP	1987	GAS	21594.73		336		COLUMBUS	JOSEPH BITTINGER JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1988	GAS	51243.65		356		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS DEWEY CORNERS	29-Dec-83 29-Dec-83
	55.50	GAS			7.5				8			
123-33914 US ENERGY DEV CORP	1989 1990	GAS	67741.18 66748.67		364 352		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1990	GAS			350		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	
123-33914 US ENERGY DEV CORP		GAS	38209				COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1992	090000000	13492		320		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1993	GAS	6206		352		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 US ENERGY DEV CORP	1994	GAS	2570		341		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 BELDEN & BLAKE CORP	2000	GAS	559		366		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 BELDEN & BLAKE CORP	2001	GAS	438		365		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 BELDEN & BLAKE CORP	2002	GAS	372		273		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 BELDEN & BLAKE CORP	2002	OIL	0		0		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 RANGE RESOURCES APPALACHIA LLC	2002	GAS	46		31		COLUMBUS	JOSEPH BITTINGER	1		DEWEY CORNERS	29-Dec-83
123-33914 RANGE RESOURCES APPALACHIA LLC	2003	GAS	257.85		182	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83

123-33914 RANGE RESOURCES APPALACHIA LLC	2004	GAS	313.84		244	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 RANGE RESOURCES APPALACHIA LLC	2005	GAS	47.28		212	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 RANGE RESOURCES APPALACHIA LLC	2006	GAS	4.33		151	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 TRINITY ENERGY CORP	2007	GAS	64		365	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 LION ENERGY CO LLC	2008	BRINE		38		WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 LION ENERGY CO LLC	2008	GAS	392		365	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
123-33914 LION ENERGY CO LLC	2009	GAS	90		120	WARREN	COLUMBUS	JOSEPH BITTINGER	1	COLUMBUS	DEWEY CORNERS	29-Dec-83
		Total	334,886	38								

Total All 7 wells 1,751,614

GEOLOGIC DATA EARTHQUAKE EPICENTERS MAP (PA DCNR)



Section 6 – Operating Data

Section 6 - Operating Data

The proposed commercial brine disposal well will primarily be utilized to inject produced and flowback water from wells completed in the Marcellus Shale, the Medina Group and other natural gas and oil producing formations. Other oil and gas related wastewaters associated with the production of oil and natural gas or natural gas storage operations, which are approved by EPA for injection under a UIC Class II D injection well, may also be injected. According to Title 40 Chapter I Sec. 144.6 (b)(1), such fluids include those "Which are brought to the surface in connection with natural gas storage operations, or conventional oil or natural gas production and may be commingled with waste waters from gas plants which are an integral part of production operations, unless those waters are classified as a hazardous waste at the time of injection."

Injection Rate

Injection rate and pressure data collected to date for the nearby Bittinger #4 permitted brine disposal well indicate the well is capable of a sustainable injection rate of approximately 1,000 bbls/day while operating within the maximum injection pressure permit limit. This is consistent with the permitted injection volume of 30,000 bbls/month for this well. (The 2014 Annual Disposal/Injection Well Monitoring Report for Bittinger #4 is attached.) Considering the proximity of the Bittinger #3 well to the Bittinger #4 well (which is located approximately 0.5 mile to the west) and the similarity in the injection interval based on log analysis, it is anticipated that the Bittinger #3 well can also be operated at this injection rate while staying below the proposed MIP. (Please see the attached Billman Geologic Consultants report and included geologic cross-sections.) An injection rate of 30,000 bbls/month is therefore also proposed for the Bittinger #3 well.

Maximum Allowable Surface Injection Pressure (MASIP) and Average Surface Injection Pressure

MASIP calculations based on EPA approved equations are included in the "Geologic Data" section of this application. Based on these calculations, the proposed MASIP is 1732 psi. It is estimated that the average surface injection pressure will be approximately 1000 psi.

Laboratory Analysis of Injection Fluid Samples

Laboratory analytical results for samples representative of the types of brine which will be injected into the proposed injection well are attached. Samples were collected from produced water generated from gas wells in the vicinity of the injection well as well as Marcellus brine from a brine processing facility.

Monitoring of Injection Fluid Samples and Well

The following identifies the UIC Class II underground injection well regulatory requirements and operational procedures which will be conducted to meet the subject requirements:

- 1. Monitoring of the nature of injected fluids at time intervals sufficiently frequent to yield data representative of their characteristics. An initial sample of fluid will be collected and analyzed from initial loads proposed for disposal from new disposal customers. In addition, samples will be collected for analysis from new types of sources (e.g., from different geologic formations, geographic regions, etc.) which would be expected to differ significantly from brine previously characterized for disposal at the facility. Samples will be analyzed for the following parameters at a minimum: specific gravity, total dissolved solids and pH.
- 2. Observation of injection pressure, flow rate, and cumulative volume at least weekly based on the regulatory requirements for produced fluid disposal operations. Injection pressures,

annular pressure, injection rate, and cumulative volume will be continuously monitored and recorded electronically.

- 3. A demonstration of mechanical integrity pursuant to 40 CFR Sec. 146.8 at least once every two years during the life of the injection well. A mechanical integrity test will be performed prior to initiating injection and at least once every two years.
- 4. **Maintenance of the results of all monitoring until the next permit review.** All monitoring records will be maintained throughout the life of the well.

Reporting requirements consist of the following:

An annual report will be submitted to EPA summarizing the results of the required monitoring, including monthly records of injected fluids, and any major changes in characteristics or sources of injected fluid.

Proposed Annulus Fluid

The proposed annulus fluid for the proposed injection well will consist of fresh water and a water soluble corrosion inhibitor. The corrosion inhibitor will be mixed in accordance with the manufacturer's recommendations then loaded into the well annulus prior to conducting injection operations. Product information for the type of corrosion inhibitor which will be utilized is attached. A similar type product may be used instead of the example product referenced.

Facility Layout and Operation

The attached drawing shows the following elements of the existing Bear Lake Properties brine disposal well facility including the recently permitted and constructed brine storage area. The brine storage facility was permitted as a residual waste transfer facility under PADEP residual waste regulations. The following key elements of the brine disposal facility are shown on the attached drawing:

- Existing permitted brine offloading facility located at the corner of State Route 4004 and State Line Road;
- The brine storage facility (located near the Bittinger #2 well) which is connected to the unloading area by underground double-walled piping; and,
- The three existing permitted UIC Class IID wells (Bittinger #1, #2 and #4) plus proposed UIC Class IID wells (Bittinger #3 and Smith-Ras Unit #1).

The brine storage facility has a capacity of 3,000 barrels and is anticipated to be operational during the First Quarter of 2015. A drawing showing details of the brine storage facility is attached.

Once the brine storage facility is operational, brine will be pumped from the offload station via the dual (secondary containment) pipeline to the storage tanks at the brine storage facility. The brine will then be pumped from the brine storage facility via high pressure dual (secondary containment) pipelines to the permitted brine disposal wells for injection.

The storage tanks in the brine storage area are located within a diked containment area with the containment area sized to account for the entire volume of the largest container, plus 10%. Automatic shut-off valves are incorporated into the tank design to prevent overflow during filling operations. The facility is surrounded by a fence having locking entrance and exit gates. A security camera is also strategically situated on the site.

OPERATING DATA TYPICAL BRINE LABORATORY ANALYSIS

® Microbac Laboratories, Inc.

BRADFORD DIVISION P.O. BOX 489 BRADFORD

PA 16701

(814)368-6087

http://www.microbac.com

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CERTIFICATE OF ANALYSIS

KCS LENAPE RESOURCES CORP.

9489 ALEXANDER ROAD

ALEXANDER

NY 14005

LAUGER- EPLANICH

Date Received 7/13/01 9931-00207 Order No 008010 Invoice No K011 Cust # .7/09/01 Sampled Date

DATE

Sampled Time

00:00

TECH

Sample Id

UNITS

RESULT

Permit No Cust P.O.

TEST

HP

LION ENERGY - BRINE SAMPLE SUBMITTED 7/13/01 Subject:

METHOD

1001					
LION ENERGY - BRT	INE SAMPLE				
BY POT SALTS IN BRINE		·	•	1/23/01	ERI
: C10#	,	. 33,600	¥G/L	1/23/01	ER I
CHLORIDE		195,000	MG/L	1/23/01	er i
POTASSIUM		1910	₩G-/ C.	7/23/01	1 8 3
NAGNESIUN	•	3330	#G/L	7/23/01	ERI
SODIUM		80,700	HG/C	7/23/01	ER I
SPECIFIC GRAVITY		1.216		7/23/01	er j
CALCIUM CHLORIDE	•	7.65	X BY WGT.	7/23/01	ERI
SODIUM CHLORIDE	•	16.82	% BY WGT.	7/23/01	ERI
POTASSIUM CHLORIDE		0.10	S by WGT.	7/23/01	er i
MAGNESIUM CHLORIDE		1.07	% by Wgt.	7/23/01	ERI
TOTAL CHLORIDES	•	25.84	A BY WGT.	7/23/01	ER I
CALCIUM CHLORIDE	•	. 0.776	LDS/GAL.	7/23/01	ER I
SODIUM CHLORIDE		1,707	LBS/GAL.	7/23/01	er i
POTASSION CHLORIDE		0.930	LBS/GAL.	7/23/01	ERI
- NAGNESSIUM CHLORIDE		0.109	LBS/GAL.	7/23/01	er i
TOTAL CHLORIDES		2.62	LBS/GAL	1/23/01	er i
WEIGHT OF 1 GALLON OF BRINE		. 10.15	LAS/GAL	7/23/01	ER I

ANALYSIS BY NYS LAB:

S. G. = 10.15 # CAL = 1.218

Certificate Of Analysis Continued On Next Page

Client Sample Results

Client: Bear Lake Properties, LLC Project/Site: Injection Well Permitting

TestAmerica Job ID: 180-17986-1

ient Sample ID: CW 011013

Date Collected: 01/10/13 13:30 Date Received: 01/11/13 09:30 Lab Sample ID: 180-17986-1

Matrix: Water

Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Barium	5200000	В	5000	44	ug/L		01/16/13 09:44	01/16/13 18:31	
iron	1600	JB	5000	230	ug/L		01/12/13 12:22	01/14/13 21:03	100
Magnesium	2300000	В	10000	200	ug/L		01/12/13 12:22	01/14/13 21:03	100
Manganese	10000	В	500	3.7	ug/L		01/12/13 12:22	01/14/13 21:03	100
Sodium	32000000	В	10000	270	ug/L		01/12/13 12:22	01/14/13 21:03	100
General Chemistry								•	
Analyte	Result	Qualifier	RL	MDL	Unit	D	Prepared	Analyzed	Dil Fac
Chloride	130000		1000	200	mg/L			01/12/13 11:36	1000
Alkalinity	6.5	В	5.0	0.41	mg/L			01/14/13 08:06	1
Bicarbonate Alkalinity as CaCO3	6.5	В	5.0	0.41	mg/L			01/14/13 08:06	1
Carbonate Alkalinity as CaCO3	ND		5.0	0.41	mg/L			01/14/13 08:06	
Hardness	74000		2500	770	mg/L			01/14/13 09:05	500
Total Dissolved Solids	200000		1000	1000	mg/L			01/11/13 14:39	1
Total Organic Carbon - Duplicates	63		40	7.5	mg/L			01/21/13 11:02	40
Analyte	Result	Qualifier	RL	RL	Unit	D	Prepared	Analyzed	Dil Fac
pH	6.23	HF	0.100	0.100	SU			01/15/13 09:50	1
Specific Conductance	440000		1600	1600	umhos/cm			01/11/13 18:45	1600
Total Solids	220000		10	10	mg/L			01/15/13 15:50	1

AQUACLEAR PRODUCT INFORMATION

558 Verbile Store Base Clusteren, 1171 (1907)-1399 1864):343-4782 Fran 3641:345-365























Corrosion Inhibitor SticksT

WHAT ARE CORROSION INHIBITOR STICKST?

Corrosion Inhibitor SticksT are water soluble or oil soluble sticks that contain a blend of Imidazolines which have excellent filming characteristics and low emulsion tendencies. This unique blend gives effective corrosion control for most oil field corrosion problems.

CORROSION INHIBITOR STICKTM USES

Corrosion Inhibitor Sticks ™ are primarily used to control common corrosion problems found in producing oil and gas well systems. They can be used to treat hard to reach 'dead' areas such as the annulus space above the packer, rat-hole, or the bottom of water supply tanks.

ADVANTAGES OF CORROSION INHIBITOR STICKST

Corrosion Inhibitor SticksT can provide corrosion control throughout the entire production system. Regular usage will help control corrosion at the point they begin - down-hole.

They are available in two different formulations (oil soluble and water dispersable) or (water soluble and oil dispersable). The oil soluble type is soluble in oil, condensate and wet gas and can slowly disperse inhibitor into the water phase. The water soluble type is soluble in water and can slowly disperse inhibitor into the oil phase.

Corrosion Inhibitor SticksT can effectively inhibit corrosion in wells that produce both water and distillate or oil phases. In this case, it may be desirable to treat the well with both types of sticks by first dropping water soluble sticks and allowing them to fall through the oil into the water, thus dissolving and releasing inhibitor in

TREATMENT DETERMINATION

The number of Corrosion Inhibitor SticksT used is based on the volume of total fluid produced (oil or condensate plus water). Field experience indicates that for most corrosive environments the best results are achieved by using a larger initial slug treatment (80 PPM daily) until the problem is under control then reduce to smaller periodic treatments (40 PPM daily) thereafter. EXAMPLE: An initial slug treatment of 80 PPM would require 0.64 lbs of Corrosion Inhibitor Stick™ per 24 BBL (1000 gallons) of total fluid produced.

COR. INH. STICK™ SIZES SENIOR (1.5/8 " x 18")	STICKS PER BBL 1 per 58 bbls
JUNIOR (1 3/8 " x 16 ") JUNIOR (1 1/4" x 15")	1 per 40 bbls
THRIFTY (1" x 15")	1 per 29 bbls 1 per 18 bbls
MIDGET (5/8" × 15")	1 per 7 bbls

NOTE: To successfully control any corrosion problem, the inhibitor insertion into the fluid stream must be constant. For intermittent treatment or extreme corrosive environments increase the number of sticks accordingly.

THE MOST COMMON PROCEDURE for producing wells is to shut-in well and drop sticks through lubricator. Leave well shut until sticks fall to the bottom. The time in minutes for the sticks to fall to the bottom (assuming well is shut-in with fluid at surface) is equal to the depth divided by 100. (Time, min. = Depth, ft / 100).

<u>FOR WATER INJECTION SYSTEMS</u> drop the sticks into the water supply tank to inhibit more of the system.

the water column). Then drop the oil soluble sticks which will "FLOAT" at where the oil and water contact thus slowly dissolving and releasing inhibitor in the oil column.

The sticks are economical when compared to conventional corrosion control operations and therefore save investment in pumps, drums of chemical, and equipment maintenance.

Corrosion Inhibitor SticksT may be used in wells with bottom hole temperatures (BHT) of up to 375 degrees Fahrenheit.

PRODUCTION SPECIFICATIONS

OIL SOLUBLE: The stick will dissolve in 20 to 120 minutes (in moving diesel) depending on temperature, salt content, and relative fluid motion. The stick will melt at 135 degrees Fahrenheit and the specific gravity is 0.95.

WATER SOLUBLE: The stick will dissolve in 12 to 24 hours (in 60,00 PPMmoving brine water) depending on temperature, salt content, and relative fluid motion. The stick will melt at 125 degrees Fahrenheit and the specific gravity is 1.10.

PRODUCT PACKAGING

SENIOR	1.55 lb/stick 24/case 31/pail 48/chest
JUNIOR(1)	1.20 lb/stick 36/case n/a 72/chest
JUNIOR(2)	0.76 lb/stick 36/case 52/pail 72/chest
THRIFTY	0.49 lb/stick 49/case 72/pail 98/chest
MIDGET	0.19 lb/stick 108/case 204/pail 216/chest

WHERE TO BUY

All good oil field supply stores carry Aqua-Clear, Inc. Corrosion Inhibitor Sticks™, but you can also buy direct from us.

Ordering Information

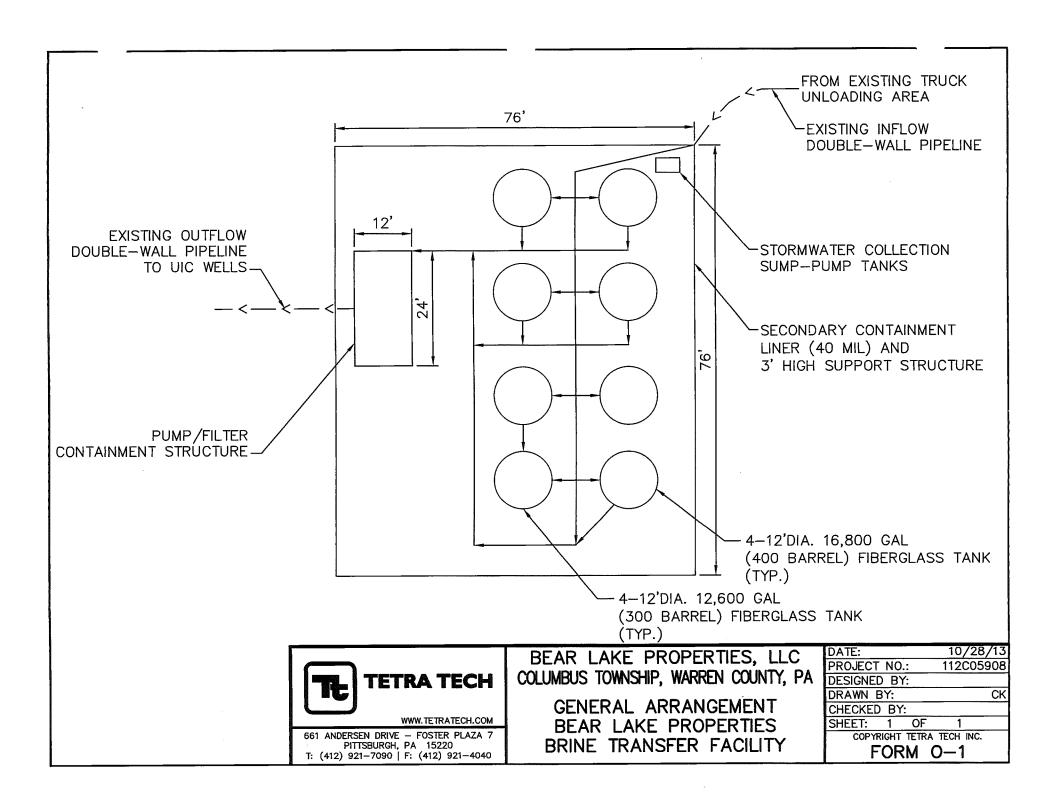
Should you wish to speak to a sales representative about any of our products, you can call or email Tommy Halloran Jr., Ronald "Buster" Wilson, or Russell Cook directly:

Tommy Halloran Jr. W 304-343-4792 H 304-345-5152 C 304-546-8526 tom@aquaclear-inc.com

Ronald "Buster" Wilson W 304-546-8518 H 304-965-7996 Fax 304-965-2713 buster@aguaclear-inc.com

Russell Cook W 304-546-2940 H 304-842-7050 Fax 304-842-7050 russell@aquaclear-inc.com

OPERATING DATA FACILITY LAYOUT SCHEMATIC



OPERATING DATA ANNUAL OPERATING DATA REPORTS

United States Environmental Protection Agency
Washington, DC 20460

ANNUAL DISPOSAL/INJECTION WELL MONITORING REPORT								
Name and Address of Ex	xisting Permittee			Name and A	ddress of Surface Owi	ner		
Bear Lake Properties, 3000 Village Run Ro	, LLC ad, Unit 103, #223, V	Vexford, PA 1509	0	Miles Sam 82530 Pan	psel gan Rd., Erie, PA 16	5509		
Locate Well and O Section Plat - 640 A	County Permit Number unsylvania Warren PAS2D215 BWAR							
Surface Location Description								
		1/4 of 1/4 of 1/4 of Section Township Range Locate well in two directions from nearest lines of guarter section and drilling unit						
		Surf	Surface					
	- -	Loca	Location ft. frm (N/S) Line of quarter section and ft. from (E/W) Line of quarter section.					
w i i		E	WELL ACTIV		TYPE OF PERMI	т		
		-	Brine Disposal Individual Enhanced Recovery Area					
	_	-	Hydroca	rbon Storage	Number of Well	s		
			Lease Name	Bittinger		Well Number 4	, , , , , , , , , , , , , , , , , , , ,	
S								
 ·	INJECTION	PRESSURE		TOTAL VOLUM	ME INJECTED		ANNULUS PRESSURE MONITORING)	
MONTH YEAR	AVERAGE PSIG	MAXIMUM PSIG		BBL	MCF	MINIMUM PSIG	MAXIMUM PSIG	
January-2014	1100	1440	8995			0	540	
February-2014	960	1130	2716			0	0	
March-2014	0	0	1474			0	0	
April-2014	1200	1460	15395			0	120	
May-2014	1500	1600	14586			80	120	
June-2014	1550	1620	12803			80	100	
July-2014	1300	1400	17838			80	100	
August-2014	1380	1400	9316			80	100	
September-2014	1540	1620	2434		Translation of	50	150	
October-2014	1580	1620	12338			60	180	
November-2014	1580	1620	9840			80	200	
December-2014	1590	1620	8559			80	200	
attachments and information is tru	e penalty of law that I I that, based on my inq Je, accurate, and comp e and imprisonment. (uiry of those indivi lete. I am aware t	amined and a iduals immed hat there are	liately respon	sible for obtaining the	information, I believe	e that the	
Name and Official Title (Please type or print)			Signature			Į p	ate Signed	
John C. Holko, Vice President							01/29/15	

OPERATING DATA TYPICAL CORROSION INHIBITOR

AQUACLEAR PRODUCT INFORMATION

808 Grabit Street Bast. Charlevon, "75 /994\3²34792 Fex (304) 3454935























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マース・ポープ アグル・ディング アル・・・・・・・・・・・・・・・ だまい・・・	TICKS PER BBL
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Grande de la companya de la companya de la companya de la companya de la companya de la companya de la companya	l per 40 bbls
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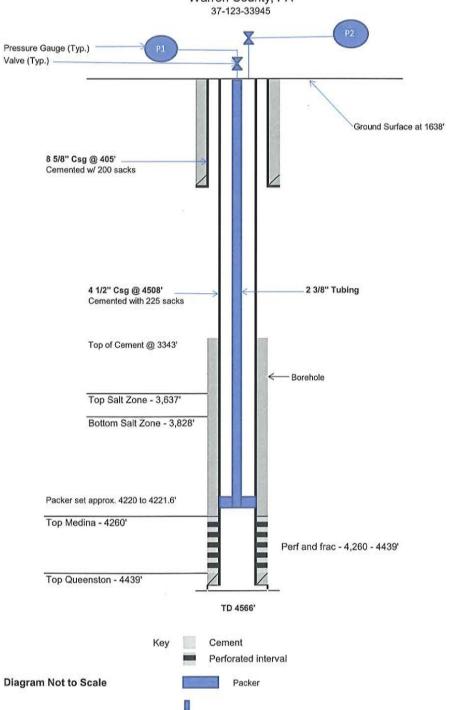
Russell Cook W 304-546-2940 H 304-842-7050 Fax 304-842-7050 russell@aquaclear-inc.com Section – 7 Well Construction Details

WELL CONSTRUCTION INJECTION WELL CONFIGURATION

Figure 1
Well Construction Diagram

Bear Lake Properties, LLC Bittinger #3

Columbus Township Warren County, PA



Tubing

Bittinger #3 Surface cement calculation:

Surface hole size: 12-1/4"*

Suface cement volume: 200 sx Class A*

Surface casing: 405ft. of 8-5/8"

Class A cement yield: 1.18 cu. ft. per sack

Annular volume between 12-1/4" O.H. and 8-5/8" casing: 0.4127 cu. ft. per ft.

Cement volume required: $405 \text{ ft.} \times 0.4127 \text{ cu. ft.}$ per ft. = 167.1 cu. ft.

Cement volume pumped: 200 sx class A x 1.18 cu. ft./sk = 236 cu. ft.

*surface casing hole size and cement type based upon detail offset well surface cement ticket of the Smith-Ras #1 well – cement ticket attached in this section. This offset well was drilled by the same operator in the same approximate time period as the Bittinger #3.

	juda ta nii.	No. 1 To Property		HE DOW CHEMIC		OR FIELD SERVICES MINING SERVICES INDUSTRIAL SERVICES	k -
WELL SERVICE OFDER.		PRESPUNDENCE.	REMITTANO	:E [C		OCATION NAME AND	JUMBER
EIFT, AND INVOICE NO.		BOX 4378 USTON, TEXAS 77210	P.O. BOX 10 HOUSTON,	00344 TEXAS 77212	CORRY	1 01-16	
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SMITH RA			BEAR LA	KA		DOWEL	L
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0 823-121	CLAS	S "A" CEM	ENT	SKS.	150	4,76	714,00
\$7005-100	5-1	DOWFLAKE	<u> </u>	18	400	,27	198.00
102-050	D46	ANTIFOAM	AGENT	123	30	2,50	75,00
14003-025				128	50.	1,22	41,00
6702-085	85/4 L	lasa Pure		EA	12.0	60,00	60.00
0101-085	85/8	GUIDE SHI	oÆ	EA	10	190,00	1190,00
6008-085	85/8 2	BASKET		EA	1 / 8	\$ 180,00	1180,00
4011-088	8 5/8	CENTRALIZ		EA	2	53,00	106,00
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WELL CONSTRUCTION BITTINGER #3 COMPLETION RECORD

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DIVISION OF OIL AFO GAS RECULATION
PITTSBURGH VEIL ACLVANIA 15222

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Columbus

WELL RECORD

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(09 & Gas Garlogy Division)

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NAME	TOP	BOTTOM	GAS AT	OIL AT	WATER AT (FRESH OR SALT WATER)	SOURCE OF DATA
Unconsolidated Gravel	۰0٠	301			Fresh at 60'	Driller's records
Devonian Shales	יסכ	28161				and geophysical
"Tully" LS	2816'	2926'				logs
Hamilton Shale	29261	3097'				
Onondaga	3097'	3256'			:	
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Akron-Bertie	32851	י 3370				
Camillus	3,370'	34421				
Syracuse	34421	3641'				
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Section 8 – Monitoring Program

Section 8 - Monitoring Program

The fluid levels in the following nearby depleted Medina natural gas wells will be measured and recorded semi-annually, at a minimum. The monitoring well locations are shown on the attached figure.

Injection Well	Monitoring Well	Approximate Distance and Direction From Injection Well
Bittinger #3	R. Craker #1	1,900 ft to the northeast
	D. Wright #1	2,000 ft to the southeast

Section 9 – Plugging and Abandonment Plan

Section 9 - Plugging and Abandonment Plan

At the point when the well is no longer used, the well will be abandoned in accordance with EPA and PADEP regulations. With regard to PADEP regulations, this currently includes providing a "Notice of Intent to Plug a Well" no less than 3 days and no more than 30 days prior to abandoning the well, to allow a PADEP inspector to be present during the plugging procedure. The PADEP may waive the notification period. The notification will include well location plat, well logs, production logs, injection logs, construction details, and proposed abandonment method. After receiving approval from PADEP to proceed, the well will be abandoned and the abandonment procedures will be documented on a "Certificate of Plugging".

The USEPA will be notified of the plugging activity at least 45 days prior to commencing activities. This notification will include USEPA Form No. 7514-20. A proposed plugging plan (Form 7514-20) is attached based on the current PADEP and USEPA regulations. However, this may be modified prior to plugging in order to meet the requirements at the time of the plugging activity. A contractor cost estimate to perform plugging and abandonment according to the proposed plugging plan is attached. The contractor estimate is approximately \$24,000 for these services.

PLUGGING AND ABANDONMENT PLAN PLUGGING AND ABANDONMENT ESTIMATED COSTS



DLH Energy Service, LLC PO Box 40 5296 Bly Hill Road Ashville, NY 14710 Phone: 716-410-0204 or 716-410-0028

Fax: 716-526-4080

www.dlhenergyservice.com

03/18/2014

Re: Plugging Estimate for the Bittinger 3 Well Columbus Twp PA

Dear Sirs,

The following is an estimate for the plugging to abandon the above mentioned well.

Rig Time:

Two twelve hour days rig at \$215/hour, crew truck \$100/day, 4th man 8 hours \$40/hr

for laying down casing, \$5,680.00

Wire line service:

Jet Cut 4 ½ casing: \$2,500.00

Cement and pumping service:

Up to 500 sacks cement and up to 140 bbls. Gel.

\$9,948.00

Water Hauling and Disposal:

Delivery of fresh water and removal of returned fluid . \$855.00

Rentals:

500 bbl. Water tank and open top returns tank 5 day minimum \$500.00

Support equipment:

Dozer at 2 days \$500.00

Trucking: mob and de mob dozer, excavator, water tank, open top, casing

and tangibles (20 hrs) \$1,900.00

Remedial Work

Pea stone plug back with delivery, tank cleaning, excavating and cutting off

surface casing, welding cap and monument, reclamation and seeding. \$1,500.00

Total \$23,383.00

If you have any questions, please feel free to contact me at (716) 410-1543.

Best Regards,

Bill Weaver

Bill Weaver
Operations Supervisor
DLH Energy Service

PLUGGING AND ABANDONMENT PLAN EPA FORM 7520-14

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Washington, DC 20460 PLUGGING AND ABANDONMENT PLAN															
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I certify under the penalty of law that I have personally examined and am familiar with the information submitted in this document and all attachments and that, based on my inquiry of those individuals immediately responsible for obtaining the information, I believe that the															
inf	Information is true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment. (Ref. 40 CFR 144.32)														
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FINAL PLUGGED WELL DRAWING

API/Permit: 37-123-33945 Bittinger #3

Pipe cut below plow depth with plate on top

Pea Gravel

Btm of surface csg 405'

Gel Spacer

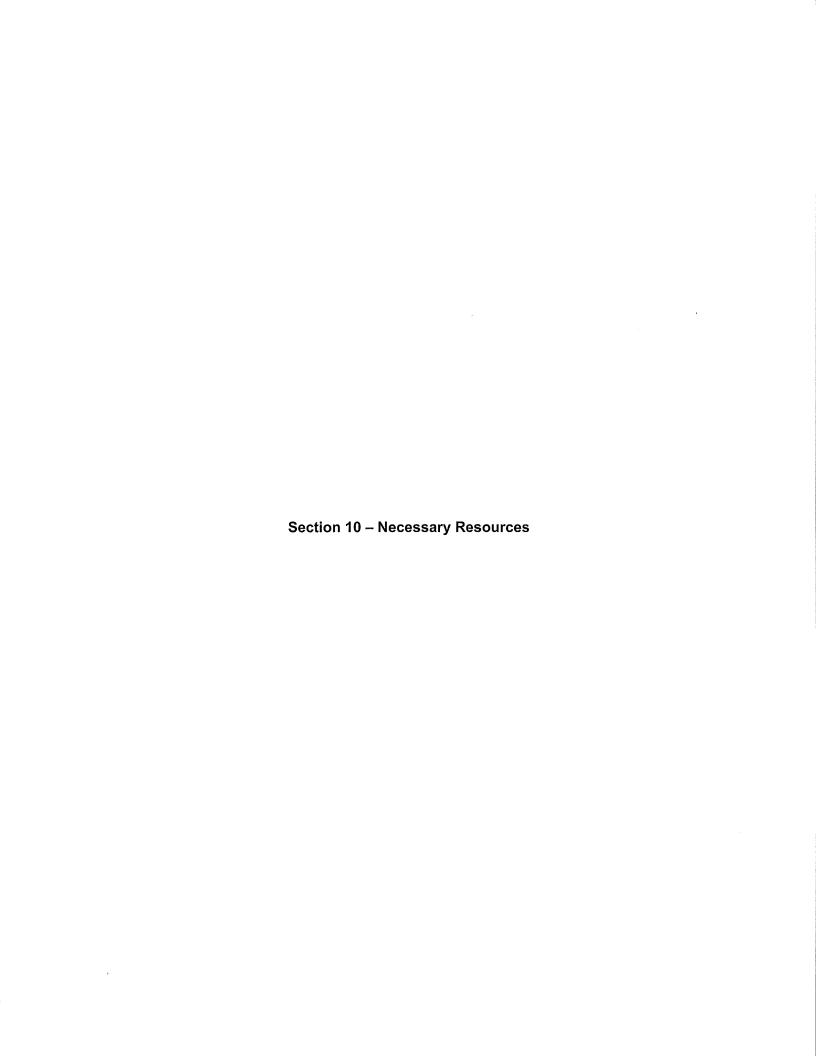
Dunkirk Shale Top approx 1,700'

518 sk cement plug 410'-460'

Total casing 4,508 ft

Capacity 4-1/2" casing	0.0895 ft3/ In- ft
Capacity 7-7/8" hole	0.3382 ft3/ In- ft
Capacity 8-5/8" casing	0.3575 ft3/ In- ft
	10.00% Excess open hole plugs
Plugging Plan	1.18 ft3/sk cement yield

Top Plug	Plug Size Ft	Cement Amnt in Sacks
0 ft		
18 ft	6	5
Bottom of Surface Casing		
410 ft		
460 ft	19	16
One Plug for Hydrocarbon Inter	vals to Cutoff Point	
1700 ft		
3343 ft	611	518
Divergence and desire interval		
Plug across producing interval		
4240 ft		
4470 ft	21	18



Section 10 - Necessary Resources





Section 11: Plans for Well Failure

General system design and monitoring: The system being utilized for monitoring and control will function with the use of pressure switch gauges with adjustable limit switches and motor valves. The gauges provide a sensing device for changes in pressure conditions and if the limit switches are reached, they will send responses to activate motor valves controlling injection flow and pressure relief. In addition to the automated portion of the system, the manual operation of all pumping equipment as well as the continual inspections of the pumping and monitoring equipment provide additional safeguards for appropriate actions necessary in case of well failures.

<u>Injection Pressure Limit Monitoring:</u> The primary safeguard to prevent over pressuring is the automated shutdown on the pumping equipment at which the maximum operating pressure can be set as a limit at which all pumping will cease.

Additional switch gauges and motor valves will be utilized at the wellhead to monitor pressure changes that would be caused by tubing or casing failures and the appropriate valve will be activated to cease injection.

<u>Tubing and Packer Monitoring:</u> With the monitoring switch gauge connected to the tubing, we will have a secondary system to prevent over pressuring of the tubing. When the maximum pressure is sensed, a response is sent to a motor valve which will stop additional injection into the tubing.

<u>Tubing to Casing Annulus Monitoring:</u> This annular space will be monitored for both increase and decreases in pressure. The switch gauge will have both a low and high shutdown tab limit. When either of the limits is reached, the sensor will send a response to a motor valve shutting down flow. The lower limit will be used to monitor damage to the casing which allows fluid to leave the casing, and the high limit will sense a pressure increase in the casing that may be caused by communication with the tubing or flow into the annular space. Both of these limits when reached will send responses shutting down the injection cycle.

<u>8-5/8" Annular Monitoring:</u> The PADEP requires the annular valve on the 8-5/8" casing head to remain open to the atmosphere at all times. We will connect this point to a storage tank capable of collecting any fluid and allowing visual monitoring of any fluid flow. The valve and associated gauge will be monitored and inspected visually for changes or fluid flow. If such is detected, the system will be shut down and the remaining equipment associated with the system will be inspected to evaluate the cause of the changes.

Under the monitoring provided above, well failures will either be identified by the automated equipment and switch gauges or by visual inspection during injection operations or at other times. Should any failure occur, all injections will cease and proper notifications to EPA will be made. Analysis of the failure will take place and the

necessary repairs to be implemented along with any equipment replacement will be coordinated with the EPA.

APPENDIX A SURROUNDING LANDOWNER INFORMATION

Landowners Within 1/4 Mile of the Bittinger #3 Well

